

**BUILDING COLLAPSE LOADS TO ACCORDING BEAM and COLUMN CAPACITY MOMENTS**

TOTAL COLUMN BASE CAPACITY MOMENT : Mrx=4226.23 (tm) Mry=4018.08 (tm)  
 TOTAL BEAM CAPACITY MOMENT : Mrx=1081.98 (tm) Mry=871.47 (tm)  
 $\sum Mc < \sum Mb > Mb = Mc$  ARRANGEMENT BEAM CAPACITY MOMENT : Mrx=1081.98 (tm) Mry=960.05 (tm)  
 X DIR. COLLAPSE CAPACITY : Px=252.43 x ( 4226.23 + 1081.98 ) / 2869.62 = 466.95 (t)  
 Y DIR. COLLAPSE CAPACITY : Py=253.79 x ( 4018.08 + 960.05 ) / 2894.44 = 436.48 (t)  
 SOFT STORY COLLAPSE CAP. : Px=2817.48 (t), Py=4262.77 (t)  
 Retrofit Project: Capacity check for E1: New R/C bars, E2-E9: Existing R/C bars  
 Vtx= $\lambda$ .Ao.I.S(t).W=858.27 (t) ( $\lambda=0.85$ )  
 Vty= $\lambda$ .Ao.I.S(t).W=862.87 (t) ( $\lambda=0.85$ )

Story no	X dir.			Y dir.		
	Column $\sum Mc$	Beam (Mci $\geq$ Mbi) $\sum Mbi$	Capacity Vr	Column $\sum Mc$	Beam (Mci $\geq$ Mbi) $\sum Mbi$	Capacity Vr
5	1023.52	164.40	395.97	1817.38	117.28	644.89
4	1095.78	391.73	309.96	1918.06	292.03	460.31
3	1152.22	620.24	263.36	1984.48	477.62	365.24
2	4102.55	878.73	563.67	3790.66	740.52	511.49
1	4226.23	1081.98	466.95	4018.08	960.05	436.48

(Mci  $\geq$  Mbi) >>  $\sum Mbi$  Beam Plastic Hinge Check

**EXISTING & RETROFITTED BUILDING COLAPSE PREVENTION COMPARISONS**

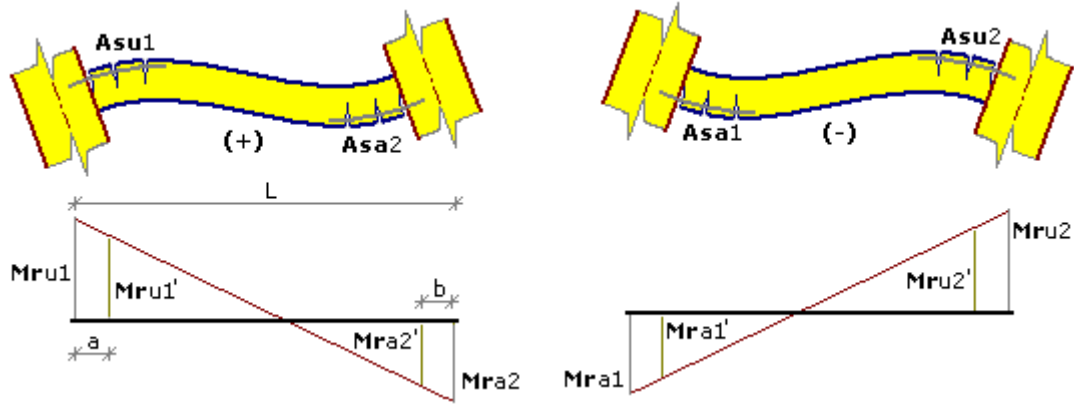
Story no	X dir.			Y dir.		
	Seismic Ve	Exist Building Vr	Retrofitted Vr	Seismic Ve	Exist Building Vr	Retrofitted Vr
5	96.57	107.89 ✓	395.97 ✓	97.91	94.25 ✗	644.89 ✓
4	161.07	120.74 ✗	309.96 ✓	163.06	100.85 ✗	460.31 ✓
3	207.10	124.02 ✗	263.36 ✓	209.27	103.99 ✗	365.24 ✓
2	238.75	126.45 ✗	563.67 ✓	240.79	106.25 ✗	511.49 ✓
1	252.16	121.64 ✗	466.95 ✓	253.83	103.03 ✗	436.48 ✓

**RETROFITTING PROJECT: COLUMNS CAPACITY SCHEDULE FOR EXISTING R/C BARS**

COLUMN min. Longitudinal reinf. ratio : 0.01

EXISTING BAR CORROSION RATIO % : 0

COLUMN NO	SIZE	COLUMN RC. BARS	As cm <sup>2</sup>	-X		+X		-Y		+Y	
				Nd	Mr	Nd	Mr	Nd	Mr	Nd	Mr
C401	25x50	2x4ø14+2x1ø14 g.	15.39	11.21	4.15	8.32	3.89	10.97	9.12	7.67	8.45
C301	25x50	2x4ø14+2x1ø14 g.	15.39	22.98	4.87	16.46	4.56	22.53	11.28	15.37	10.01
C201	25x50	2x4ø14+2x1ø14 g.	15.39	34.66	5.41	24.48	4.94	34.74	12.61	22.29	11.25
C101	25x50	2x4ø14+2x1ø14 g.	15.39	46.26	5.68	32.14	5.30	46.20	13.13	29.67	12.10
CZ01	25x60	2x3ø14+2x2ø14 g.	15.39	58.20	6.82	40.13	6.30	58.00	17.02	37.21	15.23
C402	25x50	2x4ø14+2x1ø14 g.	15.39	9.20	3.97	8.83	3.93	12.83	9.50	8.57	8.63
C302	25x50	2x4ø14+2x1ø14 g.	15.39	19.55	4.70	16.91	4.58	26.25	11.71	16.30	10.20
C202	25x50	2x4ø14+2x1ø14 g.	15.39	30.05	5.20	25.13	4.97	39.80	12.84	23.93	11.44
C102	25x60	2x3ø14+2x2ø14 g.	15.39	41.20	6.36	33.89	5.96	53.83	16.71	31.61	14.53
CZ02	25x60	2x3ø14+2x2ø14 g.	15.39	52.22	6.68	42.53	6.43	67.60	17.38	39.28	15.48
C403	50x25	2x4ø14+2x1ø14 g.	15.39	7.88	8.49	5.07	7.92	6.56	3.73	6.56	3.73
C303	50x25	2x4ø14+2x1ø14 g.	15.39	14.53	9.84	11.17	9.16	13.29	4.35	13.29	4.35
C203	50x25	2x4ø14+2x1ø14 g.	15.39	21.18	11.12	17.34	10.41	19.91	4.72	19.91	4.72
C103	50x25	2x4ø14+2x1ø14 g.	15.39	27.46	11.85	23.51	11.39	26.44	5.03	26.44	5.03
CZ03	60x25	2x3ø14+2x2ø14 g.	15.39	35.11	14.96	31.60	14.53	37.35	6.15	33.04	5.92
C404	25x50	2x4ø14+2x1ø14 g.	15.39	5.06	3.59	5.06	3.59	1.05	7.10	0.07	6.90
C304	25x50	2x4ø14+2x1ø14 g.	15.39	9.68	4.01	9.68	4.01	3.19	7.54	-1.02	6.68
C204	25x50	2x4ø14+2x1ø14 g.	15.39	16.81	4.57	16.81	4.57	8.91	8.70	1.30	7.15
C104	25x60	2x3ø14+2x2ø14 g.	15.39	2.38	3.33	2.38	3.33	-5.90	6.87	-16.18	4.34
CZ04	25x60	2x3ø14+2x2ø14 g.	15.39	4.76	3.55	4.76	3.55	-3.56	7.44	-16.77	4.20
C405	50x25	2x4ø14+2x1ø14 g.	15.39	6.76	8.26	1.98	7.29	7.82	3.84	0.11	3.13
C305	50x25	2x4ø14+2x1ø14 g.	15.39	14.31	9.80	4.75	7.85	17.89	4.62	-1.86	2.95
C205	50x25	2x4ø14+2x1ø14 g.	15.39	24.94	11.56	10.61	9.04	29.96	5.20	0.66	3.18
C105	50x30	2x4ø14+2x1ø14 g.	15.39	11.52	9.20	-7.58	5.33	19.00	6.05	-21.43	1.42
CZ05	60x30	2x4ø14+2x2ø14 g.	18.46	15.46	13.81	-7.93	8.05	21.46	7.10	-26.58	1.61
C406	50x25	2x4ø14+2x1ø14 g.	15.39	15.45	10.03	10.63	9.05	11.74	4.20	12.73	4.29
C306	50x25	2x4ø14+2x1ø14 g.	15.39	30.74	12.23	20.23	11.00	24.96	4.96	24.79	4.95
C206	50x25	2x4ø14+2x1ø14 g.	15.39	46.25	13.14	30.07	12.15	37.27	5.47	37.52	5.47
C106	60x30	2x4ø14+2x2ø14 g.	18.46	62.54	20.38	40.51	18.15	51.60	9.20	50.08	9.11
CZ06	60x30	2x4ø14+2x2ø14 g.	18.46	78.37	21.37	50.51	19.42	65.82	9.66	62.70	9.56
C407	50x25	2x4ø14+2x1ø14 g.	15.39	11.09	9.14	10.42	9.01	14.79	4.48	17.03	4.58
C307	50x25	2x4ø14+2x1ø14 g.	15.39	23.66	11.41	21.34	11.14	28.30	5.12	33.26	5.35
C207	50x25	2x4ø14+2x1ø14 g.	15.39	36.62	12.70	32.64	12.45	41.95	5.58	49.64	5.75
C107	60x30	2x4ø14+2x2ø14 g.	18.46	51.56	19.54	46.15	18.87	55.43	9.33	65.70	9.66
CZ07	60x30	2x4ø14+2x2ø14 g.	18.46	66.21	20.66	59.22	20.13	68.57	9.75	81.03	10.04
C408	25x50	2x4ø14+2x1ø14 g.	15.39	2.00	3.30	7.49	3.81	0.71	7.03	8.42	8.60
C308	25x50	2x4ø14+2x1ø14 g.	15.39	3.79	3.47	16.62	4.56	1.46	7.18	21.21	11.12
C208	25x50	2x4ø14+2x1ø14 g.	15.39	12.98	4.32	33.14	5.35	10.39	9.00	39.70	12.84



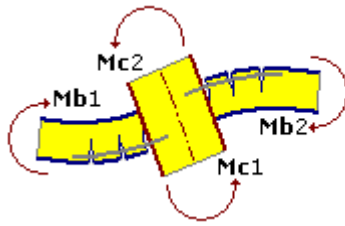
**BEAMS CAPACITY SCHEDULE**

Vlim = 0.22 Aw fcd

BEAM NO	Bw D	Ln	a b	Lft Rgt	Asu (cm <sup>2</sup> )	Asa (cm <sup>2</sup> )	Mra'	Mru'	Mg+Mq	Mra	Mru	Vd	Vr
BZ01	20	4.000	0.000	Lft	3.80	3.08	3.31	4.01 >	1.51 ✓	3.31	4.01	4.97 <	14.32 ✓
	50		0.000	Rgt	4.93	3.08	3.31	5.16 >	-1.08 ✓	3.31	5.16	3.38 <	14.32 ✓
BZ02	20	2.975	0.000	Lft	4.93	4.62	4.84	5.16 >	1.47 ✓	4.84	5.16	5.01 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	-1.24 ✓	4.84	4.01	5.05 <	14.32 ✓
BZ04	20	3.600	0.000	Lft	5.40	4.62	4.88	5.63 >	3.41 ✓	4.88	5.63	7.18 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	2.79 ✓	4.88	5.63	5.45 <	14.32 ✓
BZ05	20	3.050	0.000	Lft	5.40	6.03	6.27	5.63 >	-2.77 ✓	6.27	5.63	6.29 <	14.32 ✓
	50		0.000	Rgt	4.27	6.03	6.27	4.49 >	-3.96 ✓	6.27	4.49	8.47 <	14.32 ✓
BZ06	20	3.605	0.000	Lft	5.40	4.62	4.84	5.63 >	3.67 ✓	4.84	5.63	7.04 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	-2.35 ✓	4.84	5.63	6.31 <	14.32 ✓
BZ07	20	3.000	0.000	Lft	12.57	6.28	6.52	12.80 >	-3.99 ✓	6.52	12.80	11.10 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	0.02 ✓	6.52	18.31	9.21 <	17.25 ✓
BZ07	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	2.68 ✓	6.52	18.31	17.13 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	-2.68 ✓	6.52	18.31	17.12 <	17.25 ✓
BZ08	20	3.900	0.000	Lft	3.80	3.08	3.28	4.01 >	1.59 ✓	3.28	4.01	4.49 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-2.51 ✓	3.28	5.57	4.98 <	14.32 ✓
BZ09	20	4.550	0.000	Lft	5.34	3.08	3.28	5.57 >	2.12 ✓	3.28	5.57	4.45 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-2.36 ✓	3.28	5.57	4.51 <	14.32 ✓
BZ10	20	5.850	0.000	Lft	9.36	3.08	3.31	9.56 >	7.06 ✓	3.31	9.56	7.98 <	14.32 ✓
	50		0.000	Rgt	8.48	3.08	3.31	8.71 >	-1.01 ✓	3.31	8.71	3.35 <	14.32 ✓
BZ11	20	3.005	0.000	Lft	8.48	2.26	2.45	8.67 >	2.04 ✓	2.45	8.67	5.58 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-2.38 ✓	2.45	4.01	6.21 <	14.32 ✓
BZ12	20	3.745	0.000	Lft	3.80	3.08	3.28	4.01 >	1.07 ✓	3.28	4.01	4.22 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.01 ✓	3.28	5.57	3.51 <	14.32 ✓
BZ13	20	3.595	0.000	Lft	5.40	4.62	4.88	5.63 >	2.07 ✓	4.88	5.63	6.78 <	14.32 ✓
	50		0.000	Rgt	6.28	4.62	4.88	6.52 >	-0.05 ✓	4.88	6.52	3.97 <	14.32 ✓
BZ14	20	2.250	0.000	Lft	6.28	4.62	4.88	6.52 >	2.70 ✓	4.88	6.52	8.17 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.88	4.01 >	-2.76 ✓	4.88	4.01	8.41 <	14.32 ✓
BZ15	20	3.000	0.000	Lft	3.80	4.62	4.84	4.01 >	0.53 ✓	4.84	4.01	5.72 <	19.77 ✓
	50		0.000	Rgt	6.54	4.62	4.84	6.78 >	3.10 ✓	4.84	6.78	8.12 <	19.77 ✓
BZ16	20	3.455	0.000	Lft	6.54	6.28	6.52	6.78 >	-2.56 ✓	6.52	6.78	4.11 <	14.32 ✓
	50		0.000	Rgt	7.42	6.28	6.52	7.67 >	-2.76 ✓	6.52	7.67	7.45 <	14.32 ✓
BZ17	20	4.030	0.000	Lft	4.62	3.08	3.28	4.84 >	1.36 ✓	3.28	4.84	6.08 <	14.32 ✓
	50		0.000	Rgt	5.75	3.08	3.28	5.98 >	-0.16 ✓	3.28	5.98	3.31 <	14.32 ✓
BZ18	20	1.945	0.000	Lft	5.75	2.26	2.45	5.98 >	1.46 ✓	2.45	5.98	10.20 <	14.32 ✓
	50		0.000	Rgt	12.51	2.26	2.45	12.31 >	7.56 ✓	2.45	12.31	55.23 >	14.32 ✗
BZ21	20	2.255	0.000	Lft	3.80	4.62	4.84	4.01 >	1.05 ✓	4.84	4.01	6.27 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	-1.31 ✓	4.84	5.63	6.55 <	14.32 ✓
BZ22	20	4.000	0.000	Lft	4.93	3.08	3.31	5.16 >	2.35 ✓	3.31	5.16	5.33 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.31	4.01 >	-1.49 ✓	3.31	4.01	3.78 <	14.32 ✓
BZ23	20	2.975	0.000	Lft	3.80	4.62	4.84	4.01 >	1.05 ✓	4.84	4.01	4.60 <	14.32 ✓
	50		0.000	Rgt	4.93	4.62	4.84	5.16 >	-1.60 ✓	4.84	5.16	6.24 <	14.32 ✓
BZ25	20	3.600	0.000	Lft	5.40	4.62	4.88	5.63 >	4.35 ✓	4.88	5.63	7.82 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	-3.02 ✓	4.88	5.63	7.53 <	14.32 ✓
BZ26	20	2.900	0.000	Lft	3.80	6.03	6.27	4.01 >	-2.76 ✓	6.27	4.01	6.71 <	14.32 ✓
	50		0.000	Rgt	5.40	6.03	6.27	5.63 >	-2.58 ✓	6.27	5.63	8.03 <	14.32 ✓
BZ27	20	3.605	0.000	Lft	5.40	4.62	4.84	5.63 >	2.39 ✓	4.84	5.63	6.35 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	-3.56 ✓	4.84	5.63	7.01 <	14.32 ✓
BZ28	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	-0.02 ✓	6.52	18.31	15.10 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	3.98 ✓	6.52	18.31	16.99 <	17.25 ✓
BZ28	20	2.900	0.000	Lft	18.85	6.28	6.52	18.31 >	-3.96 ✓	6.52	18.31	10.67 <	17.25 ✓
	50		0.000	Rgt	12.57	6.28	6.52	12.80 >	-2.68 ✓	6.52	12.80	11.52 <	17.25 ✓
BZ29	20	3.900	0.000	Lft	5.34	3.08	3.28	5.57 >	1.74 ✓	3.28	5.57	4.63 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-2.36 ✓	3.28	4.01	4.83 <	14.32 ✓
BZ30	20	4.550	0.000	Lft	5.34	3.08	3.28	5.57 >	2.47 ✓	3.28	5.57	4.60 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.57 ✓	3.28	5.57	4.21 <	14.32 ✓
BZ31	20	5.850	0.000	Lft	9.36	3.08	3.31	9.56 >	6.85 ✓	3.31	9.56	7.95 <	14.32 ✓
	50		0.000	Rgt	8.48	3.08	3.31	8.71 >	-0.91 ✓	3.31	8.71	3.23 <	14.32 ✓
BZ32	20	3.005	0.000	Lft	8.48	2.26	2.45	8.67 >	2.31 ✓	2.45	8.67	5.70 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-2.48 ✓	2.45	4.01	6.27 <	14.32 ✓

BEAM NO	Bw D	Ln	a b	Lft Rgt	Asu (cm <sup>2</sup> )	Asa (cm <sup>2</sup> )	Mra'	Mru'	Mg+Mq	Mra	Mru	Vd	Vr
B136	20	3.025	0.000	Lft	3.80	4.62	4.84	4.01 >	0.27 ✓	4.84	4.01	5.23 <	19.77 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	3.36 ✓	4.84	5.63	7.85 <	19.77 ✓
B137	20	3.455	0.000	Lft	5.40	6.28	6.52	5.63 >	-2.87 ✓	6.52	5.63	4.93 <	14.32 ✓
	50		0.000	Rgt	8.55	6.28	6.52	8.81 >	-2.88 ✓	6.52	8.81	7.92 <	14.32 ✓
B139	20	1.950	0.000	Lft	4.21	2.26	2.45	4.42 >	-0.05 ✓	2.45	4.42	8.22 <	14.32 ✓
	50		0.000	Rgt	12.51	2.26	2.45	12.31 >	6.69 ✓	2.45	12.31	32.19 >	14.32 ✗
B142	20	3.050	0.000	Lft	2.26	4.62	4.84	2.45 >	-1.83 ✓	4.84	2.45	4.17 <	14.32 ✓
	50		0.000	Rgt	2.26	4.62	4.84	2.45 >	1.81 ✓	4.84	2.45	26.02 >	14.32 ✗
B143	20	2.750	0.000	Lft	3.80	4.62	4.84	4.01 >	-1.63 ✓	4.84	4.01	5.01 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	-1.31 ✓	4.84	4.01	4.79 <	14.32 ✓
B201	20	4.000	0.000	Lft	3.80	3.08	3.31	4.01 >	1.56 ✓	3.31	4.01	4.70 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.31	4.01 >	-1.86 ✓	3.31	4.01	4.03 <	14.32 ✓
B202	20	2.975	0.000	Lft	3.80	4.62	4.84	4.01 >	1.26 ✓	4.84	4.01	4.47 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	1.58 ✓	4.84	4.01	4.76 <	14.32 ✓
B204	20	3.700	0.000	Lft	5.40	4.62	4.88	5.63 >	3.11 ✓	4.88	5.63	7.10 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	3.33 ✓	4.88	5.63	6.28 <	14.32 ✓
B205	20	3.025	0.000	Lft	5.40	6.03	6.27	5.63 >	-3.32 ✓	6.27	5.63	5.42 <	14.32 ✓
	50		0.000	Rgt	3.80	6.03	6.27	4.01 <	-4.29 ✗	6.27	4.01	8.84 <	14.32 ✓
B206	20	3.705	0.000	Lft	5.81	3.08	3.28	6.04 >	4.19 ✓	3.28	6.04	7.14 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.64 ✓	3.28	4.01	5.76 <	14.32 ✓
B207	20	3.000	0.000	Lft	12.57	6.28	6.52	12.80 >	-4.43 ✓	6.52	12.80	10.73 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	-3.96 ✓	6.52	18.31	11.63 <	17.25 ✓
B207	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	0.29 ✓	6.52	18.31	14.63 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	-0.26 ✓	6.52	18.31	14.63 <	17.25 ✓
B208	20	3.950	0.000	Lft	3.80	3.08	3.28	4.01 >	1.59 ✓	3.28	4.01	4.57 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-2.81 ✓	3.28	5.57	5.09 <	14.32 ✓
B209	20	4.525	0.000	Lft	5.34	3.08	3.28	5.57 >	1.76 ✓	3.28	5.57	4.32 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.68 ✓	3.28	5.57	4.30 <	14.32 ✓
B210	20	5.875	0.000	Lft	11.69	6.28	6.56	11.96 >	6.56 ✓	6.56	11.96	8.56 <	14.32 ✓
	50		0.000	Rgt	8.55	6.28	6.56	8.81 >	-1.30 ✓	6.56	8.81	4.04 <	14.32 ✓
B211	20	3.005	0.000	Lft	8.55	2.26	2.45	8.73 >	2.13 ✓	2.45	8.73	4.61 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-2.66 ✓	2.45	4.01	5.49 <	14.32 ✓
B212	20	3.820	0.000	Lft	3.80	3.08	3.28	4.01 >	0.90 ✓	3.28	4.01	4.12 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.30 ✓	3.28	5.57	3.56 <	14.32 ✓
B213	20	3.695	0.000	Lft	5.40	4.62	4.88	5.63 >	1.53 ✓	4.88	5.63	6.64 <	14.32 ✓
	50		0.000	Rgt	6.28	4.62	4.88	6.52 >	0.87 ✓	4.88	6.52	3.53 <	14.32 ✓
B214	20	2.175	0.000	Lft	6.28	4.62	4.88	6.52 >	4.46 ✓	4.88	6.52	9.88 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.88	4.01 >	-2.99 ✓	4.88	4.01	8.93 <	14.32 ✓
B215	20	3.000	0.000	Lft	3.80	4.62	4.84	4.01 >	-0.14 ✓	4.84	4.01	5.32 <	19.77 ✓
	50		0.000	Rgt	6.28	4.62	4.84	6.52 >	3.60 ✓	4.84	6.52	8.14 <	19.77 ✓
B216	20	3.580	0.000	Lft	6.28	4.02	4.23	6.52 >	-3.09 ✓	4.23	6.52	3.53 <	14.32 ✓
	50		0.000	Rgt	7.42	4.02	4.23	7.66 >	-2.99 ✓	4.23	7.66	6.99 <	14.32 ✓
B218	20	1.970	0.000	Lft	4.21	2.26	2.45	4.42 >	0.63 ✓	2.45	4.42	8.01 <	14.32 ✓
	50		0.000	Rgt	9.36	2.26	2.45	9.50 >	7.25 ✓	2.45	9.50	12.06 <	14.32 ✓
B221	20	2.355	0.000	Lft	3.80	4.62	4.84	4.01 >	1.74 ✓	4.84	4.01	7.27 <	14.32 ✓
	50		0.000	Rgt	6.28	4.62	4.84	6.52 >	-0.48 ✓	4.84	6.52	6.23 <	14.32 ✓
B222	20	4.000	0.000	Lft	3.80	3.08	3.31	4.01 >	2.27 ✓	3.31	4.01	5.02 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.31	4.01 >	-1.21 ✓	3.31	4.01	3.30 <	14.32 ✓
B223	20	2.975	0.000	Lft	3.80	4.62	4.84	4.01 >	1.88 ✓	4.84	4.01	5.20 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	-1.60 ✓	4.84	4.01	5.87 <	14.32 ✓
B225	20	3.700	0.000	Lft	5.40	4.62	4.88	5.63 >	4.18 ✓	4.88	5.63	7.68 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	-3.35 ✓	4.88	5.63	8.24 <	14.32 ✓
B226	20	2.900	0.000	Lft	3.80	6.03	6.27	4.01 >	-3.34 ✓	6.27	4.01	7.50 <	14.32 ✓
	50		0.000	Rgt	5.40	6.03	6.27	5.63 >	-3.23 ✓	6.27	5.63	8.43 <	14.32 ✓
B227	20	3.655	0.000	Lft	3.80	4.62	4.84	4.01 >	1.52 ✓	4.84	4.01	5.98 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	-4.27 ✓	4.84	5.63	7.45 <	14.32 ✓
B228	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	3.93 ✓	6.52	18.31	16.69 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	4.47 ✓	6.52	18.31	15.76 <	17.25 ✓
B228	20	2.900	0.000	Lft	18.85	6.28	6.52	18.31 >	-4.46 ✓	6.52	18.31	11.09 <	17.25 ✓
	50		0.000	Rgt	12.57	6.28	6.52	12.80 >	-0.26 ✓	6.52	12.80	9.85 <	17.25 ✓
B229	20	3.925	0.000	Lft	5.34	3.08	3.28	5.57 >	1.38 ✓	3.28	5.57	4.44 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.68 ✓	3.28	4.01	4.60 <	14.32 ✓
B230	20	4.525	0.000	Lft	5.34	3.08	3.28	5.57 >	2.83 ✓	3.28	5.57	4.82 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.93 ✓	3.28	5.57	4.43 <	14.32 ✓
B231	20	5.900	0.000	Lft	8.48	3.08	3.31	8.71 >	6.40 ✓	3.31	8.71	7.72 <	14.32 ✓
	50		0.000	Rgt	8.48	3.08	3.31	8.71 >	-1.39 ✓	3.31	8.71	3.47 <	14.32 ✓
B232	20	2.980	0.000	Lft	8.48	4.62	4.84	8.74 >	1.61 ✓	4.84	8.74	6.15 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	-3.02 ✓	4.84	4.01	7.32 <	14.32 ✓
B233	20	3.770	0.000	Lft	3.80	3.08	3.28	4.01 >	0.80 ✓	3.28	4.01	3.99 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.39 ✓	3.28	5.57	3.78 <	14.32 ✓
B234	20	3.695	0.000	Lft	5.40	4.62	4.88	5.63 >	1.58 ✓	4.88	5.63	6.66 <	14.32 ✓
	50		0.000	Rgt	6.28	4.62	4.88	6.52 >	1.10 ✓	4.88	6.52	3.74 <	14.32 ✓
B235	20	2.175	0.000	Lft	6.28	4.62	4.88	6.52 >	4.66 ✓	4.88	6.52	10.08 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.88	4.01 >	-3.05 ✓	4.88	4.01	8.98 <	14.32 ✓
B236	20	3.025	0.000	Lft	3.80	4.62	4.84	4.01 >	-0.31 ✓	4.84	4.01	5.22 <	19.77 ✓
	50		0.000	Rgt	6.54	4.62	4.84	6.78 >	3.33 ✓	4.84	6.78	8.40 <	19.77 ✓
B237	20	3.555	0.000	Lft	6.54	6.28	6.52	6.78 >	-2.79 ✓	6.52	6.78	3.78 <	14.32 ✓
	50		0.000	Rgt	6.94	6.28	6.52	7.19 >	-3.05 ✓	6.52	7.19	7.48 <	14.32 ✓
B239	20	1.975	0.000	Lft	4.21	4.62	4.84	4.42 >	0.63 ✓	4.84	4.42	9.29 <	14.32 ✓
	50		0.000	Rgt	9.36	4.62	4.84	9.62 >	7.26 ✓	4.84	9.62	13.35 <	14.32 ✓
B242	20	3.050	0.000	Lft	2.26	4.62	4.84	2.45 >	-1.95 ✓	4.84	2.45	4.22 <	14.32 ✓
	50		0.000	Rgt	2.26	4.62	4.84	2.45 >	2.00 ✓	4.84	2.45	13.07 <	14.32 ✓

BEAM NO	Bw D	Ln	a b	Lft Rgt	Asu (cm <sup>2</sup> )	Asa (cm <sup>2</sup> )	Mra'	Mru'	Mg+Mq	Mra	Mru	Vd	Vr
B405	20	3.025	0.000	Lft	5.40	6.03	6.27	5.63 >	-3.54 ✓	6.27	5.63	4.15 <	14.32 ✓
	50		0.000	Rgt	3.80	6.03	6.27	4.01 <	-4.40 ✗	6.27	4.01	7.91 <	14.32 ✓
B406	20	3.705	0.000	Lft	5.34	3.08	3.28	5.57 >	3.72 ✓	3.28	5.57	6.96 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.34 ✓	3.28	4.01	5.68 <	14.32 ✓
B407	20	3.000	0.000	Lft	12.57	6.28	6.52	12.80 >	-4.32 ✓	6.52	12.80	8.08 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	-2.59 ✓	6.52	18.31	6.68 <	17.25 ✓
B407	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	2.08 ✓	6.52	18.31	7.95 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	-2.09 ✓	6.52	18.31	7.97 <	17.25 ✓
B408	20	3.950	0.000	Lft	3.80	3.08	3.28	4.01 >	1.16 ✓	3.28	4.01	3.73 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-2.96 ✓	3.28	5.57	4.40 <	14.32 ✓
B409	20	4.525	0.000	Lft	5.34	3.08	3.28	5.57 >	1.64 ✓	3.28	5.57	3.20 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.59 ✓	3.28	5.57	3.19 <	14.32 ✓
B410	20	5.875	0.000	Lft	7.42	6.28	6.56	7.67 >	5.75 ✓	6.56	7.67	7.33 <	14.32 ✓
	50		0.000	Rgt	7.42	6.28	6.56	7.67 >	-1.14 ✓	6.56	7.67	2.59 <	14.32 ✓
B411	20	3.005	0.000	Lft	7.42	2.26	2.45	7.64 >	2.94 ✓	2.45	7.64	3.38 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-2.32 ✓	2.45	4.01	3.83 <	14.32 ✓
B412	20	3.820	0.000	Lft	3.80	3.08	3.28	4.01 >	0.97 ✓	3.28	4.01	3.42 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.14 ✓	3.28	4.01	2.43 <	14.32 ✓
B413	20	3.695	0.000	Lft	3.80	4.62	4.88	4.01 >	1.08 ✓	4.88	4.01	5.58 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	1.46 ✓	4.88	5.63	3.57 <	14.32 ✓
B414	20	2.175	0.000	Lft	5.40	4.62	4.88	5.63 <	5.68 ✗	4.88	5.63	8.35 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.88	4.01 >	-3.14 ✓	4.88	4.01	6.80 <	14.32 ✓
B415	20	3.000	0.000	Lft	3.80	4.62	4.84	4.01 >	-0.71 ✓	4.84	4.01	3.03 <	19.77 ✓
	50		0.000	Rgt	6.28	4.62	4.84	6.52 >	3.70 ✓	4.84	6.52	6.19 <	19.77 ✓
B416	20	3.580	0.000	Lft	6.28	4.02	4.23	6.52 >	-3.18 ✓	4.23	6.52	2.35 <	14.32 ✓
	50		0.000	Rgt	6.28	4.02	4.23	6.52 >	-3.14 ✓	4.23	6.52	6.23 <	14.32 ✓
B418	20	1.970	0.000	Lft	4.21	2.26	2.45	4.42 >	0.64 ✓	2.45	4.42	6.55 <	14.32 ✓
	50		0.000	Rgt	6.22	2.26	2.45	6.45 <	7.42 ✗	2.45	6.45	18.06 >	14.32 ✗
B421	20	2.405	0.000	Lft	3.80	4.62	4.84	4.01 >	1.37 ✓	4.84	4.01	6.71 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.84	5.63 >	-0.53 ✓	4.84	5.63	6.01 <	14.32 ✓
B422	20	4.000	0.000	Lft	3.80	3.08	3.31	4.01 >	2.15 ✓	3.31	4.01	4.74 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.31	4.01 >	-1.46 ✓	3.31	4.01	2.98 <	14.32 ✓
B423	20	2.975	0.000	Lft	3.80	2.26	2.45	4.01 >	1.96 ✓	2.45	4.01	3.88 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-1.13 ✓	2.45	4.01	4.52 <	14.32 ✓
B425	20	3.700	0.000	Lft	5.40	4.62	4.88	5.63 >	4.18 ✓	4.88	5.63	7.61 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	-3.31 ✓	4.88	5.63	8.21 <	14.32 ✓
B426	20	2.900	0.000	Lft	3.80	6.03	6.27	4.01 >	-3.60 ✓	6.27	4.01	6.48 <	14.32 ✓
	50		0.000	Rgt	5.40	6.03	6.27	5.63 >	-2.82 ✓	6.27	5.63	7.15 <	14.32 ✓
B427	20	3.705	0.000	Lft	3.80	3.08	3.28	4.01 >	1.33 ✓	3.28	4.01	5.67 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-3.73 ✓	3.28	5.57	6.96 <	14.32 ✓
B428	20	1.500	0.000	Lft	18.85	6.28	6.52	18.31 >	2.56 ✓	6.52	18.31	8.33 <	17.25 ✓
	50		0.000	Rgt	18.85	6.28	6.52	18.31 >	4.33 ✓	6.52	18.31	9.75 <	17.25 ✓
B428	20	2.900	0.000	Lft	18.85	6.28	6.52	18.31 >	-4.31 ✓	6.52	18.31	7.94 <	17.25 ✓
	50		0.000	Rgt	12.57	6.28	6.52	12.80 >	-2.09 ✓	6.52	12.80	6.46 <	17.25 ✓
B429	20	3.950	0.000	Lft	5.34	3.08	3.28	5.57 >	1.49 ✓	3.28	5.57	3.90 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.59 ✓	3.28	4.01	3.80 <	14.32 ✓
B430	20	4.525	0.000	Lft	5.34	3.08	3.28	5.57 >	2.95 ✓	3.28	5.57	3.80 <	14.32 ✓
	50		0.000	Rgt	5.34	3.08	3.28	5.57 >	-1.26 ✓	3.28	5.57	3.18 <	14.32 ✓
B431	20	5.900	0.000	Lft	7.42	6.28	6.56	7.67 >	5.70 ✓	6.56	7.67	7.44 <	14.32 ✓
	50		0.000	Rgt	8.55	6.28	6.56	8.81 >	-1.15 ✓	6.56	8.81	2.83 <	14.32 ✓
B432	20	2.980	0.000	Lft	8.55	2.26	2.45	8.73 >	2.65 ✓	2.45	8.73	3.52 <	14.32 ✓
	50		0.000	Rgt	3.80	2.26	2.45	4.01 >	-2.29 ✓	2.45	4.01	4.07 <	14.32 ✓
B433	20	3.820	0.000	Lft	3.80	3.08	3.28	4.01 >	1.00 ✓	3.28	4.01	3.44 <	14.32 ✓
	50		0.000	Rgt	3.80	3.08	3.28	4.01 >	-1.15 ✓	3.28	4.01	2.52 <	14.32 ✓
B434	20	3.695	0.000	Lft	3.80	4.62	4.88	4.01 >	1.14 ✓	4.88	4.01	5.60 <	14.32 ✓
	50		0.000	Rgt	5.40	4.62	4.88	5.63 >	1.64 ✓	4.88	5.63	3.71 <	14.32 ✓
B435	20	2.175	0.000	Lft	5.40	4.62	4.88	5.63 <	5.81 ✗	4.88	5.63	8.48 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.88	4.01 >	-3.36 ✓	4.88	4.01	6.93 <	14.32 ✓
B436	20	3.000	0.000	Lft	3.80	4.62	4.84	4.01 >	-0.90 ✓	4.84	4.01	2.90 <	19.77 ✓
	50		0.000	Rgt	6.28	4.62	4.84	6.52 >	3.62 ✓	4.84	6.52	6.32 <	19.77 ✓
B437	20	3.580	0.000	Lft	6.28	4.02	4.23	6.52 >	-3.09 ✓	4.23	6.52	2.46 <	14.32 ✓
	50		0.000	Rgt	6.28	4.02	4.23	6.52 >	-3.36 ✓	4.23	6.52	6.36 <	14.32 ✓
B439	20	1.975	0.000	Lft	4.21	2.26	2.45	4.42 >	0.64 ✓	2.45	4.42	6.56 <	14.32 ✓
	50		0.000	Rgt	6.22	2.26	2.45	6.45 <	7.42 ✗	2.45	6.45	18.12 >	14.32 ✗
B442	20	3.050	0.000	Lft	2.26	4.62	4.84	2.45 >	-1.96 ✓	4.84	2.45	4.22 <	14.32 ✓
	50		0.000	Rgt	2.26	4.62	4.84	2.45 >	1.97 ✓	4.84	2.45	16.20 >	14.32 ✗
B443	20	2.750	0.000	Lft	3.80	4.62	4.84	4.01 >	-1.60 ✓	4.84	4.01	4.78 <	14.32 ✓
	50		0.000	Rgt	3.80	4.62	4.84	4.01 >	-1.46 ✓	4.84	4.01	4.56 <	14.32 ✓



$M_{c1} + M_{c2} \geq M_{b1} + M_{b2} \rightarrow R_b = 1$

$M_{c1} + M_{c2} < M_{b1} + M_{b2} \rightarrow R_b = \frac{M_{b1} + M_{b2}}{M_{c1} + M_{c2}}$

$M_{rb1} = R_b \times M_{b1}$

$M_{rb2} = R_b \times M_{b2}$

**COLUMN-BEAM JOINTS MOMENT CAPACITY CHECK**

COLUMN NO	(-X)			(+X)			(-Y)			(+Y)		
	$\Sigma M_c$	$\Sigma M_b >$	$\Sigma M_b$	$\Sigma M_c$	$\Sigma M_b >$	$\Sigma M_b$	$\Sigma M_c$	$\Sigma M_b >$	$\Sigma M_b$	$\Sigma M_c$	$\Sigma M_b >$	$\Sigma M_b$
C101	12.49	> 4.01	4.01	11.60	> 3.31	3.31	30.16	> 9.56	9.56	27.33	> 3.31	3.31
C201	11.08	> 4.01	4.01	10.24	> 3.31	3.31	25.75	> 8.71	8.71	23.35	> 3.31	3.31
C102	13.04	> 8.47	8.47	12.39	> 9.99	9.99	34.09	> 5.63	5.63	30.01	> 4.88	4.88
C106	41.76	> 5.63	5.63	37.58	> 4.88	4.88	18.86	> 11.99	11.99	18.67	> 11.16	11.16
C301	10.27	> 4.01	4.01	9.49	> 3.31	3.31	23.89	> 11.96	11.96	21.26	> 6.56	6.56
C202	11.56	> 8.47	8.47	10.93	> 9.99	9.99	29.55	> 6.52	6.52	25.97	> 4.88	4.88
C206	33.52	> 5.63	5.63	30.30	> 4.88	4.88	14.67	> 11.99	11.99	14.58	> 11.16	11.16
C103	26.81	> 8.85	8.85	25.92	> 8.85	8.85	11.18	> 4.84	4.84	10.95	> 3.28	3.28
C129	64.00	> 0.00	0.00	64.00	> 0.00	0.00	160.84	> 11.40	11.40	160.84	> 11.40	11.40
C107	40.21	> 16.14	10.51	39.00	> 18.17	11.90	19.08	> 8.88	8.88	19.70	> 8.85	8.85
C109	38.09	> 5.63	5.63	32.43	> 4.84	4.84	16.80	> 6.46	6.46	17.19	> 7.29	7.29
C401	9.02	> 4.01	4.01	8.44	> 3.31	3.31	20.40	> 9.56	9.56	18.46	> 3.31	3.31
C302	9.91	> 7.32	7.32	9.55	> 8.85	8.85	24.55	> 5.63	5.63	21.64	> 4.88	4.88
C306	25.36	> 5.63	5.63	23.15	> 4.88	4.88	10.43	< 15.30	10.43	10.43	< 11.26	10.41
C203	22.97	> 12.85	8.85	21.80	> 13.68	8.85	9.75	> 0.00	0.00	9.75	> 0.00	0.00
C229	38.41	> 0.00	0.00	38.41	> 0.00	0.00	94.12	> 11.40	11.40	92.57	> 11.40	11.40
C207	32.24	> 16.14	10.51	31.32	> 18.17	11.90	14.91	> 8.88	8.88	15.41	> 8.85	8.85
C209	30.72	> 5.63	5.63	26.32	> 4.84	4.84	13.22	> 6.46	6.46	13.41	> 7.29	7.29
C130	119.24	> 2.45	2.45	119.24	> 4.84	4.84	103.79	> 9.26	9.26	103.79	> 8.43	8.43
C117	25.92	> 8.85	8.85	26.90	> 8.85	8.85	11.18	> 4.84	4.84	10.95	> 3.28	3.28
C110	39.63	> 4.84	4.84	42.26	> 5.63	5.63	19.25	> 18.39	11.61	19.05	< 19.82	13.30
C111	16.44	> 4.01	4.01	13.47	> 3.28	3.28	28.52	> 3.28	3.28	34.93	> 5.57	5.57
C501	4.15	> 4.01	4.01	3.89	> 3.31	3.31	9.12	> 7.67	7.67	8.45	> 6.56	6.56
C402	8.67	> 7.32	7.32	8.51	< 8.85	8.50	21.20	> 5.63	5.63	18.83	> 4.88	4.88
C406	22.26	> 5.63	5.63	20.05	> 4.88	4.88	9.16	< 10.90	9.17	9.25	< 10.04	9.20
C303	20.96	> 12.85	8.85	19.57	> 13.68	8.85	9.07	> 0.00	0.00	9.07	> 0.00	0.00
C304	8.59	> 0.00	0.00	8.59	> 0.00	0.00	16.23	> 11.40	11.40	13.83	> 11.40	11.40
C307	24.10	> 16.14	10.51	23.59	> 18.17	11.90	10.69	> 8.88	8.88	11.11	> 8.85	8.85
C309	23.44	> 6.04	6.04	19.87	> 3.28	3.28	9.69	> 6.46	6.46	9.75	> 7.29	7.29
C210	32.06	> 4.84	4.84	34.22	> 4.01	4.01	14.96	< 16.10	10.47	14.85	< 18.68	12.16
C211	12.85	> 4.01	4.01	10.75	> 3.28	3.28	22.99	> 3.28	3.28	28.24	> 5.57	5.57
C230	80.26	> 4.89	2.45	77.75	> 9.68	4.84	62.99	> 4.42	4.42	60.98	> 2.45	2.45
C133	108.71	> 12.54	12.54	108.71	> 8.97	8.97	136.78	> 2.45	2.45	136.78	> 12.31	12.31
C131	131.97	> 4.84	4.84	131.97	> 2.45	2.45	102.59	> 9.26	9.26	102.59	> 8.43	8.43
C116	12.37	> 9.99	9.99	13.01	> 8.47	8.47	34.07	> 5.63	5.63	29.95	> 4.88	4.88
C217	21.81	> 13.68	13.68	23.01	> 12.85	12.85	9.75	> 0.00	0.00	9.75	> 0.00	0.00
C112	18.31	> 8.84	8.84	18.48	> 8.84	8.84	35.27	> 13.05	13.05	41.17	> 15.33	15.33
C502	3.97	< 7.32	3.97	3.93	< 6.46	3.93	9.50	> 4.01	4.01	8.63	> 4.88	4.88
C506	10.03	> 4.49	4.49	9.05	> 4.88	4.88	4.20	< 14.21	4.20	4.29	< 10.11	4.26
C403	18.33	> 12.85	8.85	17.08	> 13.68	8.85	8.07	> 0.00	0.00	8.07	> 0.00	0.00
C404	7.60	> 0.00	0.00	7.60	> 0.00	0.00	14.64	> 10.51	10.51	13.58	> 10.51	10.51
C407	20.55	> 16.14	10.51	20.15	> 18.17	11.90	9.60	> 8.88	8.88	9.94	> 8.85	8.85
C409	20.07	> 7.18	7.18	17.39	> 3.28	3.28	8.65	> 6.46	6.46	8.60	> 7.29	7.29
C310	24.31	> 3.28	3.28	25.96	> 4.01	4.01	10.68	< 17.88	10.65	10.59	< 14.99	10.59
C311	9.37	> 4.01	4.01	8.12	> 3.28	3.28	17.67	> 3.28	3.28	21.21	> 5.57	5.57
C233	65.49	> 12.54	12.54	66.52	> 8.02	8.02	87.44	> 2.45	2.45	91.27	> 12.31	12.31
C212	14.29	> 8.84	8.84	14.43	> 8.84	8.84	28.71	> 13.05	13.05	32.92	> 17.62	17.62
C305	21.35	> 4.89	2.45	16.90	> 9.68	4.84	9.82	> 4.42	4.42	6.13	> 2.45	2.45
C231	84.16	> 9.68	9.68	86.64	> 4.89	4.89	61.81	> 4.42	4.42	59.63	> 2.45	2.45
C134	108.79	> 8.02	4.01	108.79	> 12.54	6.27	136.86	> 2.45	2.45	136.86	> 12.31	12.31
C115	12.21	> 3.31	3.31	13.37	> 4.01	4.01	33.20	> 9.56	9.56	29.63	> 3.31	3.31
C216	10.92	> 8.85	8.85	11.54	> 7.32	7.32	29.52	> 6.52	6.52	25.92	> 4.88	4.88
C132	55.62	> 0.00	0.00	55.62	> 0.00	0.00	152.80	> 11.40	11.40	152.80	> 11.40	11.40
C317	19.58	> 13.68	13.68	20.97	> 12.85	12.85	9.07	> 0.00	0.00	9.07	> 0.00	0.00
C127	36.09	> 31.35	31.35	34.18	< 43.14	43.14	2679.14	> 0.00	0.00	1486.26	> 0.00	0.00
C114	11.51	> 8.84	8.84	11.51	> 8.84	8.84	24.57	> 4.84	4.84	30.84	> 5.63	5.63
C503	8.49	< 10.46	6.45	7.92	< 13.68	7.92	3.73	> 0.00	0.00	3.73	> 0.00	0.00
C504	3.59	> 0.00	0.00	3.59	> 0.00	0.00	7.10	< 10.51	7.10	6.90	< 10.51	6.67
C507	9.14	< 16.14	9.15	9.01	< 18.17	8.97	4.48	< 8.88	4.46	4.58	< 8.85	4.57
C509	8.96	> 5.57	5.57	8.07	> 3.28	3.28	4.01	< 6.46	3.85	3.95	< 7.29	3.95
C410	21.13	> 3.28	3.28	23.03	> 4.01	4.01	9.56	< 17.88	9.49	9.38	< 14.99	9.38
C411	8.29	> 4.01	4.01	7.42	> 3.28	3.28	16.16	> 3.28	3.28	18.21	> 5.16	5.16
C308	7.79	< 12.54	12.54	9.91	> 8.02	8.02	16.19	> 2.45	2.45	23.96	> 9.50	9.50
C312	10.25	> 8.84	8.84	10.35	> 8.84	8.84	21.86	> 8.46	8.46	24.78	> 15.33	15.33
C104	6.88	> 0.00	0.00	6.88	> 0.00	0.00	14.31	> 0.00	0.00	8.54	> 0.00	0.00
C105	23.02	> 0.00	0.00	13.38	> 0.00	0.00	13.15	> 0.00	0.00	3.03	> 0.00	0.00
C227	33.94	> 31.35	31.35	32.71	< 43.14	43.14	1740.94	> 0.00	0.00	1229.50	> 0.00	0.00
C214	10.13	> 8.84	8.84	10.13	> 8.84	8.84	20.94	> 4.84	4.84	26.36	> 5.63	5.63
C405	18.06	> 4.89	2.45	15.14	> 9.68	4.84	8.47	> 4.42	4.42	6.08	> 4.84	4.84
C319	16.99	> 9.68	9.68	21.42	> 4.89	4.89	9.89	> 4.42	4.42	6.05	> 4.84	4.84

COLUMN NO	(-X)			(X)			(-Y)			(Y)		
	$\sum Mc$	$\sum Mb$	$> \sum Mb$	$\sum Mc$	$\sum Mb$	$> \sum Mb$	$\sum Mc$	$\sum Mb$	$> \sum Mb$	$\sum Mc$	$\sum Mb$	$> \sum Mb$
C524	10.50	> 4.01	4.01	9.61	> 3.28	3.28	4.45	< 17.88	4.40	4.34	< 14.99	4.34
	$\sum Mb= 1081.98$			$\sum Mb= 1117.22$			$\sum Mb= 871.47$			$\sum Mb= 960.05$		

**COLUMNS r CAPACITY RATIO**

COLUMN	dir	N	V	N/ (Ac.fc)	V/ (Ac.fct)	Md	Mr	r	Damage Limit
CZ01	-X	58.20	2.76	0.32	0.15	2.12	6.82	0.31	Immediate Occupancy
	+X	40.13	2.54	0.22	0.14	2.12	6.30	0.34	
	Conf.✓ -Y	58.00	8.23	0.32	0.45	15.31	17.02	0.90	
	+Y	37.21	6.58	0.21	0.36	15.31	15.23	1.01	
CZ02	-X	52.22	2.86	0.29	0.16	2.74	6.68	0.41	Immediate Occupancy
	+X	42.53	2.79	0.24	0.15	2.74	6.43	0.43	
	Conf.✓ -Y	67.60	7.41	0.38	0.41	11.66	17.38	0.67	
	+Y	39.28	6.59	0.22	0.36	11.66	15.48	0.75	
CZ03	-X	35.11	6.57	0.20	0.36	9.90	14.96	0.66	Immediate Occupancy
	+X	31.60	6.40	0.18	0.35	9.90	14.53	0.68	
	Conf.✓ -Y	37.35	3.12	0.21	0.17	3.33	6.15	0.54	
	+Y	33.04	2.81	0.18	0.15	3.33	5.92	0.56	
CZ04	-X	4.76	1.18	0.03	0.07	0.00	3.55	0.00	Immediate Occupancy
	+X	4.76	1.18	0.03	0.07	0.00	3.55	0.00	
	Conf.✓ -Y	-3.56	2.48	-0.02	0.14	0.00	7.44	0.00	
	+Y	-16.77	1.40	-0.09	0.08	0.00	4.20	0.00	
CZ05	-X	15.46	4.60	0.07	0.21	0.00	13.81	0.00	Immediate Occupancy
	+X	-7.93	2.68	-0.04	0.12	0.00	8.05	0.00	
	Conf.✓ -Y	21.46	2.37	0.10	0.11	0.00	7.10	0.00	
	+Y	-26.58	0.54	-0.12	0.02	0.00	1.61	0.00	
CZ06	-X	78.37	8.63	0.36	0.40	22.68	21.37	1.06	Immediate Occupancy
	+X	50.51	7.84	0.23	0.36	22.68	19.42	1.17	
	Conf.✓ -Y	65.82	4.28	0.30	0.20	7.17	9.66	0.74	
	+Y	62.70	4.21	0.29	0.19	7.17	9.56	0.75	
CZ07	-X	66.21	9.11	0.31	0.42	26.92	20.66	1.30	Immediate Occupancy
	+X	59.22	9.00	0.27	0.41	26.92	20.13	1.34	
	Conf.✓ -Y	68.57	4.25	0.32	0.19	6.50	9.75	0.67	
	+Y	81.03	4.36	0.38	0.20	6.50	10.04	0.65	
CZ08	-X	-13.63	1.03	-0.06	0.05	0.00	3.09	0.00	Immediate Occupancy
	+X	21.23	2.36	0.10	0.11	0.00	7.07	0.00	
	Conf.✓ -Y	-16.23	2.00	-0.08	0.09	0.00	6.01	0.00	
	+Y	36.11	5.87	0.17	0.27	0.00	17.60	0.00	
CZ09	-X	53.58	8.02	0.25	0.37	34.23	19.70	1.74	Immediate Occupancy
	+X	28.79	6.79	0.13	0.31	34.23	16.67	2.05	
	Conf.✓ -Y	42.27	3.59	0.20	0.16	7.57	8.63	0.88	
	+Y	46.22	3.70	0.21	0.17	7.57	8.87	0.85	
CZ10	-X	61.66	8.27	0.29	0.38	34.57	20.32	1.70	Immediate Occupancy
	+X	86.46	8.74	0.40	0.40	34.57	21.41	1.61	
	Conf.✓ -Y	72.12	7.89	0.33	0.36	6.00	9.87	0.61	
	+Y	68.45	7.80	0.32	0.36	6.00	9.75	0.62	
CZ11	-X	39.58	3.79	0.18	0.17	15.08	8.47	1.78	Immediate Occupancy
	+X	20.30	3.12	0.09	0.14	15.08	6.97	2.16	
	Conf.✓ -Y	19.21	6.39	0.09	0.29	16.15	14.73	1.10	
	+Y	39.16	8.03	0.18	0.37	16.15	17.98	0.90	
CZ12	-X	58.17	4.78	0.27	0.22	17.59	9.42	1.87	Immediate Occupancy
	+X	60.19	4.81	0.28	0.22	17.59	9.48	1.85	
	Conf.✓ -Y	40.13	8.76	0.19	0.40	12.27	18.11	0.68	
	+Y	72.86	10.26	0.34	0.47	12.27	21.17	0.58	
CZ13	-X	2.75	4.52	0.01	0.18	18.66	5.65	3.30	Life Safety
	+X	2.77	4.52	0.01	0.18	18.66	5.65	3.30	
	Conf.✓ -Y	55.39	10.99	0.22	0.43	11.72	26.55	0.44	
	+Y	12.48	7.41	0.05	0.29	11.72	17.42	0.67	
CZ14	-X	39.49	3.75	0.22	0.21	11.50	6.26	1.84	Immediate Occupancy
	+X	39.47	3.75	0.22	0.21	11.50	6.26	1.84	
	Conf.✓ -Y	24.42	5.59	0.14	0.31	9.55	13.63	0.70	
	+Y	67.33	7.11	0.37	0.39	9.55	17.38	0.55	

COLUMN	dir	N	V	N/ (Ac. fc)	V/ (Ac. fct)	Md	Mr	r	Damage Limit
C121 Conf.✓	-X	44.14	10.41	0.25	0.57	45.92	15.97	2.87	Life Safety
	+X	50.55	9.25	0.28	0.51	45.92	16.46	2.79	Life Safety
	-Y	54.78	4.31	0.30	0.24	13.15	6.74	1.95	Immediate Occupancy
	+Y	65.16	4.29	0.36	0.24	13.15	6.98	1.88	Immediate Occupancy
C122 Conf.✓	-X	16.21	0.00	0.09	0.00	2.22	4.60	0.48	Immediate Occupancy
	+X	-12.44	0.00	-0.07	0.00	2.22	1.97	1.13	Immediate Occupancy
	-Y	-16.13	0.00	-0.09	0.00	10.78	4.35	2.48	Immediate Occupancy
	+Y	26.67	0.00	0.15	0.00	10.78	13.91	0.77	Immediate Occupancy
C123 Conf.✓	-X	24.03	2.79	0.11	0.13	38.60	15.92	2.42	Immediate Occupancy
	+X	44.06	3.43	0.20	0.16	38.60	18.60	2.07	Immediate Occupancy
	-Y	30.74	4.21	0.14	0.19	21.09	7.93	2.66	Immediate Occupancy
	+Y	39.81	4.10	0.18	0.19	21.09	8.48	2.49	Immediate Occupancy
C124 Conf.✓	-X	70.51	3.01	0.33	0.14	40.96	20.99	1.95	Immediate Occupancy
	+X	50.47	2.91	0.23	0.13	40.96	19.42	2.11	Immediate Occupancy
	-Y	57.64	7.52	0.27	0.34	17.26	9.40	1.84	Immediate Occupancy
	+Y	54.09	7.43	0.25	0.34	17.26	9.29	1.86	Immediate Occupancy
C125 Conf.✓	-X	16.64	1.57	0.08	0.07	19.30	6.55	2.95	Immediate Occupancy
	+X	32.08	2.13	0.15	0.10	19.30	8.01	2.41	Immediate Occupancy
	-Y	16.20	1.80	0.07	0.08	27.47	13.99	1.96	Immediate Occupancy
	+Y	31.82	3.06	0.15	0.14	27.47	17.05	1.61	Immediate Occupancy
C126 Conf.✓	-X	47.46	3.88	0.26	0.21	20.82	6.57	3.17	Life Safety
	+X	45.41	3.88	0.25	0.21	20.82	6.53	3.19	Life Safety
	-Y	31.10	7.66	0.17	0.42	25.24	14.46	1.74	Immediate Occupancy
	+Y	56.85	9.58	0.32	0.53	25.24	16.93	1.49	Immediate Occupancy
C201 Conf.✓	-X	34.66	1.47	0.23	0.10	6.13	5.41	1.13	Immediate Occupancy
	+X	24.48	1.21	0.16	0.08	6.13	4.94	1.24	Immediate Occupancy
	-Y	34.74	3.23	0.23	0.21	10.42	12.61	0.83	Immediate Occupancy
	+Y	22.29	1.57	0.15	0.10	10.42	11.25	0.93	Immediate Occupancy
C202 Conf.✓	-X	30.05	2.82	0.20	0.19	9.16	5.20	1.76	Immediate Occupancy
	+X	25.13	3.97	0.17	0.26	9.16	4.97	1.84	Immediate Occupancy
	-Y	39.80	1.98	0.27	0.13	14.10	12.84	1.10	Immediate Occupancy
	+Y	23.93	1.61	0.16	0.11	14.10	11.44	1.23	Immediate Occupancy
C203 Conf.✓	-X	21.18	4.35	0.14	0.29	16.50	11.12	1.48	Immediate Occupancy
	+X	17.34	4.63	0.12	0.31	16.50	10.41	1.58	Immediate Occupancy
	-Y	19.91	0.00	0.13	0.00	0.52	4.72	0.11	Immediate Occupancy
	+Y	19.91	0.00	0.13	0.00	0.52	4.72	0.11	Immediate Occupancy
C204 Conf.✓	-X	16.81	0.00	0.11	0.00	2.11	4.57	0.46	Immediate Occupancy
	+X	16.81	0.00	0.11	0.00	2.11	4.57	0.46	Immediate Occupancy
	-Y	8.91	5.47	0.06	0.36	20.06	8.70	2.31	Immediate Occupancy
	+Y	1.30	4.85	0.01	0.32	20.06	7.15	2.81	Immediate Occupancy
C205 Conf.✓	-X	24.94	3.05	0.17	0.20	10.26	11.56	0.89	Immediate Occupancy
	+X	10.61	5.79	0.07	0.38	10.26	9.04	1.13	Immediate Occupancy
	-Y	29.96	2.52	0.20	0.17	10.83	5.20	2.08	Immediate Occupancy
	+Y	0.66	1.39	0.00	0.09	10.83	3.18	3.40	Life Safety
C206 Conf.✓	-X	46.25	1.91	0.31	0.13	16.88	13.14	1.28	Immediate Occupancy
	+X	30.07	1.65	0.20	0.11	16.88	12.15	1.39	Immediate Occupancy
	-Y	37.27	3.81	0.25	0.25	11.50	5.47	2.10	Immediate Occupancy
	+Y	37.52	3.70	0.25	0.24	11.50	5.47	2.10	Immediate Occupancy
C207 Conf.✓	-X	36.62	5.50	0.24	0.36	26.92	12.70	2.12	Immediate Occupancy
	+X	32.64	6.20	0.22	0.41	26.92	12.45	2.16	Immediate Occupancy
	-Y	41.95	2.93	0.28	0.19	10.37	5.58	1.86	Immediate Occupancy
	+Y	49.64	2.92	0.33	0.19	10.37	5.75	1.80	Immediate Occupancy
C208 Conf.✓	-X	12.98	3.45	0.09	0.23	7.80	4.32	1.81	Immediate Occupancy
	+X	33.14	3.55	0.22	0.23	7.80	5.35	1.46	Immediate Occupancy
	-Y	10.39	1.54	0.07	0.10	11.51	9.00	1.28	Immediate Occupancy
	+Y	39.70	7.09	0.26	0.47	11.51	12.84	0.90	Immediate Occupancy
C209 Conf.✓	-X	31.63	2.09	0.21	0.14	20.72	12.33	1.68	Immediate Occupancy
	+X	18.01	1.40	0.12	0.09	20.72	10.55	1.96	Immediate Occupancy
	-Y	26.86	2.09	0.18	0.14	11.97	5.05	2.37	Immediate Occupancy
	+Y	27.73	2.36	0.18	0.16	11.97	5.09	2.35	Immediate Occupancy
C210 Conf.✓	-X	37.72	1.40	0.25	0.09	21.82	12.75	1.71	Immediate Occupancy
	+X	51.35	1.42	0.34	0.09	21.82	13.37	1.63	Immediate Occupancy
	-Y	42.01	4.46	0.28	0.29	9.60	5.58	1.72	Immediate Occupancy
	+Y	40.99	4.44	0.27	0.29	9.60	5.55	1.73	Immediate Occupancy

COLUMN	dir	N	V	N/ (Ac. fc)	V/ (Ac. fct)	Md	Mr	r	Damage Limit
C301 Conf.✓	-X	22.98	1.59	0.15	0.11	6.77	4.87	1.39	Immediate Occupancy
	+X	16.46	1.32	0.11	0.09	6.77	4.56	1.49	Immediate Occupancy
	-Y	22.53	4.15	0.15	0.27	9.84	11.28	0.87	Immediate Occupancy
	+Y	15.37	1.99	0.10	0.13	9.84	10.01	0.98	Immediate Occupancy
C302 Conf.✓	-X	19.55	3.47	0.13	0.23	9.94	4.70	2.11	Immediate Occupancy
	+X	16.91	3.66	0.11	0.24	9.94	4.58	2.17	Immediate Occupancy
	-Y	26.25	2.20	0.17	0.15	13.86	11.71	1.18	Immediate Occupancy
	+Y	16.30	1.90	0.11	0.13	13.86	10.20	1.36	Immediate Occupancy
C303 Conf.✓	-X	14.53	5.13	0.10	0.34	18.34	9.84	1.86	Immediate Occupancy
	+X	11.17	5.46	0.07	0.36	18.34	9.16	2.00	Immediate Occupancy
	-Y	13.29	0.00	0.09	0.00	0.94	4.35	0.22	Immediate Occupancy
	+Y	13.29	0.00	0.09	0.00	0.94	4.35	0.22	Immediate Occupancy
C304 Conf.✓	-X	9.68	0.00	0.06	0.00	1.06	4.01	0.26	Immediate Occupancy
	+X	9.68	0.00	0.06	0.00	1.06	4.01	0.26	Immediate Occupancy
	-Y	3.19	4.58	0.02	0.30	23.48	7.54	3.12	Life Safety
	+Y	-1.02	4.58	-0.01	0.30	23.48	6.68	3.52	Life Safety
C305 Conf.✓	-X	14.31	2.20	0.10	0.15	6.52	9.80	0.67	Immediate Occupancy
	+X	4.75	4.36	0.03	0.29	6.52	7.85	0.83	Immediate Occupancy
	-Y	17.89	1.89	0.12	0.12	14.52	4.62	3.14	Life Safety
	+Y	-1.86	1.51	-0.01	0.10	14.52	2.95	4.92	Life Safety
C306 Conf.✓	-X	30.74	2.34	0.20	0.15	17.73	12.23	1.45	Immediate Occupancy
	+X	20.23	2.03	0.13	0.13	17.73	11.00	1.61	Immediate Occupancy
	-Y	24.96	3.97	0.17	0.26	11.53	4.96	2.32	Immediate Occupancy
	+Y	24.79	3.96	0.17	0.26	11.53	4.95	2.33	Immediate Occupancy
C307 Conf.✓	-X	23.66	6.62	0.16	0.44	27.11	11.41	2.38	Immediate Occupancy
	+X	21.34	8.08	0.14	0.53	27.11	11.14	2.43	Immediate Occupancy
	-Y	28.30	3.85	0.19	0.25	10.09	5.12	1.97	Immediate Occupancy
	+Y	33.26	3.94	0.22	0.26	10.09	5.35	1.88	Immediate Occupancy
C308 Conf.✓	-X	3.79	2.78	0.03	0.18	9.99	3.47	2.88	Immediate Occupancy
	+X	16.62	3.63	0.11	0.24	9.99	4.56	2.19	Immediate Occupancy
	-Y	1.46	1.59	0.01	0.10	6.90	7.18	0.96	Immediate Occupancy
	+Y	21.21	3.96	0.14	0.26	6.90	11.12	0.62	Immediate Occupancy
C309 Conf.✓	-X	21.09	2.84	0.14	0.19	20.32	11.11	1.83	Immediate Occupancy
	+X	11.95	1.40	0.08	0.09	20.32	9.32	2.18	Immediate Occupancy
	-Y	18.30	2.57	0.12	0.17	11.82	4.64	2.54	Immediate Occupancy
	+Y	18.51	3.40	0.12	0.22	11.82	4.65	2.54	Immediate Occupancy
C310 Conf.✓	-X	25.05	1.39	0.17	0.09	21.39	11.57	1.85	Immediate Occupancy
	+X	34.19	1.70	0.23	0.11	21.39	12.59	1.70	Immediate Occupancy
	-Y	28.03	4.09	0.19	0.27	9.57	5.11	1.87	Immediate Occupancy
	+Y	26.61	4.03	0.18	0.27	9.57	5.04	1.90	Immediate Occupancy
C311 Conf.✓	-X	15.23	1.68	0.10	0.11	11.84	4.50	2.63	Immediate Occupancy
	+X	8.31	1.38	0.06	0.09	11.84	3.89	3.05	Life Safety
	-Y	7.75	1.29	0.05	0.08	11.68	8.46	1.38	Immediate Occupancy
	+Y	14.86	2.12	0.10	0.14	11.68	9.91	1.18	Immediate Occupancy
C312 Conf.✓	-X	22.59	3.88	0.15	0.26	17.54	4.85	3.62	Life Safety
	+X	23.95	3.93	0.16	0.26	17.54	4.91	3.57	Life Safety
	-Y	16.86	3.35	0.11	0.22	12.48	10.32	1.21	Immediate Occupancy
	+Y	27.49	8.04	0.18	0.53	12.48	11.85	1.05	Immediate Occupancy
C313 Conf.✓	-X	1.41	2.60	0.01	0.17	20.04	3.25	6.17	Collapse Prevention
	+X	1.42	2.60	0.01	0.17	20.04	3.25	6.16	Collapse Prevention
	-Y	20.94	1.45	0.14	0.10	15.85	11.09	1.43	Immediate Occupancy
	+Y	3.56	1.76	0.02	0.12	15.85	7.61	2.08	Immediate Occupancy
C314 Conf.✓	-X	15.68	3.62	0.10	0.24	17.15	4.52	3.79	Life Safety
	+X	15.68	3.62	0.10	0.24	17.15	4.52	3.79	Life Safety
	-Y	10.38	1.88	0.07	0.12	16.66	9.00	1.85	Immediate Occupancy
	+Y	27.76	2.97	0.19	0.20	16.66	11.88	1.40	Immediate Occupancy
C315 Conf.✓	-X	16.35	1.32	0.11	0.09	6.80	4.55	1.49	Immediate Occupancy
	+X	22.86	1.60	0.15	0.11	6.80	4.86	1.40	Immediate Occupancy
	-Y	22.74	3.84	0.15	0.25	10.61	11.30	0.94	Immediate Occupancy
	+Y	15.22	1.39	0.10	0.09	10.61	9.98	1.06	Immediate Occupancy
C316 Conf.✓	-X	16.96	3.66	0.11	0.24	9.95	4.58	2.17	Immediate Occupancy
	+X	19.60	3.47	0.13	0.23	9.95	4.71	2.11	Immediate Occupancy
	-Y	26.14	2.26	0.17	0.15	13.69	11.69	1.17	Immediate Occupancy
	+Y	16.19	1.96	0.11	0.13	13.69	10.18	1.35	Immediate Occupancy



COLUMN	dir	N	V	N/ (Ac. fc)	V/ (Ac. fct)	Md	Mr	r	Damage Limit
C407 Conf.✓	-X	11.09	6.72	0.07	0.44	28.03	9.14	3.07	Life Safety
	+X	10.42	7.21	0.07	0.48	28.03	9.01	3.11	Life Safety
	-Y	14.79	3.58	0.10	0.24	9.48	4.48	2.12	Immediate Occupancy
	+Y	17.03	3.67	0.11	0.24	9.48	4.58	2.07	Immediate Occupancy
C408 Conf.✓	-X	2.00	2.64	0.01	0.17	8.87	3.30	2.68	Immediate Occupancy
	+X	7.49	3.05	0.05	0.20	8.87	3.81	2.33	Immediate Occupancy
	-Y	0.71	1.75	0.00	0.12	3.58	7.03	0.51	Immediate Occupancy
	+Y	8.42	4.11	0.06	0.27	3.58	8.60	0.42	Immediate Occupancy
C409 Conf.✓	-X	10.19	3.43	0.07	0.23	19.17	8.96	2.14	Immediate Occupancy
	+X	5.84	1.86	0.04	0.12	19.17	8.07	2.37	Immediate Occupancy
	-Y	9.65	2.98	0.06	0.20	11.24	4.01	2.80	Immediate Occupancy
	+Y	8.95	3.16	0.06	0.21	11.24	3.95	2.85	Immediate Occupancy
C410 Conf.✓	-X	13.14	1.86	0.09	0.12	20.39	9.56	2.13	Immediate Occupancy
	+X	17.49	2.28	0.12	0.15	20.39	10.45	1.95	Immediate Occupancy
	-Y	14.44	3.56	0.10	0.24	9.09	4.45	2.04	Immediate Occupancy
	+Y	13.26	3.47	0.09	0.23	9.09	4.34	2.09	Immediate Occupancy
C411 Conf.✓	-X	7.27	2.20	0.05	0.15	10.16	3.79	2.68	Immediate Occupancy
	+X	4.43	1.97	0.03	0.13	10.16	3.53	2.88	Immediate Occupancy
	-Y	3.98	2.10	0.03	0.14	13.79	7.70	1.79	Immediate Occupancy
	+Y	6.97	2.85	0.05	0.19	13.79	8.31	1.66	Immediate Occupancy
C412 Conf.✓	-X	10.82	3.29	0.07	0.22	14.62	4.12	3.55	Life Safety
	+X	11.90	3.37	0.08	0.22	14.62	4.22	3.47	Life Safety
	-Y	8.96	5.34	0.06	0.35	15.64	8.71	1.80	Immediate Occupancy
	+Y	13.15	7.65	0.09	0.51	15.64	9.56	1.64	Immediate Occupancy
C413 Conf.✓	-X	1.86	2.63	0.01	0.17	17.30	3.29	5.25	Life Safety
	+X	1.87	2.63	0.01	0.17	17.30	3.29	5.25	Life Safety
	-Y	9.19	2.46	0.06	0.16	21.09	8.76	2.41	Immediate Occupancy
	+Y	1.16	2.96	0.01	0.20	21.09	7.12	2.96	Immediate Occupancy
C414 Conf.✓	-X	7.92	3.08	0.05	0.20	14.90	3.85	3.87	Life Safety
	+X	7.92	3.08	0.05	0.20	14.90	3.85	3.87	Life Safety
	-Y	5.19	2.95	0.03	0.20	22.04	7.94	2.77	Immediate Occupancy
	+Y	13.22	4.11	0.09	0.27	22.04	9.58	2.30	Immediate Occupancy
C415 Conf.✓	-X	8.27	2.29	0.06	0.15	8.23	3.88	2.12	Immediate Occupancy
	+X	11.16	2.55	0.07	0.17	8.23	4.15	1.98	Immediate Occupancy
	-Y	11.06	5.41	0.07	0.36	12.81	9.14	1.40	Immediate Occupancy
	+Y	7.56	3.23	0.05	0.21	12.81	8.42	1.52	Immediate Occupancy
C416 Conf.✓	-X	8.85	3.15	0.06	0.21	10.58	3.94	2.69	Immediate Occupancy
	+X	9.22	3.18	0.06	0.21	10.58	3.97	2.66	Immediate Occupancy
	-Y	12.78	2.72	0.09	0.18	16.61	9.49	1.75	Immediate Occupancy
	+Y	8.52	2.91	0.06	0.19	16.61	8.62	1.93	Immediate Occupancy
C417 Conf.✓	-X	5.08	6.30	0.03	0.42	22.53	7.92	2.85	Immediate Occupancy
	+X	7.88	6.34	0.05	0.42	22.53	8.49	2.65	Immediate Occupancy
	-Y	6.56	0.00	0.04	0.00	1.29	3.73	0.35	Immediate Occupancy
	+Y	6.56	0.00	0.04	0.00	1.29	3.73	0.35	Immediate Occupancy
C418 Conf.✓	-X	5.03	0.00	0.03	0.00	0.42	3.58	0.12	Immediate Occupancy
	+X	5.03	0.00	0.03	0.00	0.42	3.58	0.12	Immediate Occupancy
	-Y	0.90	4.86	0.01	0.32	24.11	7.07	3.41	Life Safety
	+Y	-0.07	4.78	0.00	0.32	24.11	6.87	3.51	Life Safety
C419 Conf.✓	-X	2.06	4.13	0.01	0.27	3.39	7.31	0.46	Immediate Occupancy
	+X	6.83	2.57	0.05	0.17	3.39	8.28	0.41	Immediate Occupancy
	-Y	7.86	2.43	0.05	0.16	15.49	3.85	4.03	Life Safety
	+Y	0.17	1.95	0.00	0.13	15.49	3.14	4.94	Life Safety
C420 Conf.✓	-X	10.76	2.87	0.06	0.16	22.00	9.05	2.43	Immediate Occupancy
	+X	15.87	3.31	0.09	0.18	22.00	10.08	2.18	Immediate Occupancy
	-Y	12.22	4.22	0.07	0.23	15.60	5.28	2.96	Immediate Occupancy
	+Y	13.11	4.30	0.07	0.24	15.60	5.38	2.90	Immediate Occupancy
C421 Conf.✓	-X	10.00	7.14	0.07	0.47	28.33	8.92	3.18	Life Safety
	+X	10.59	6.68	0.07	0.44	28.33	9.04	3.13	Life Safety
	-Y	14.63	3.58	0.10	0.24	9.29	4.47	2.08	Immediate Occupancy
	+Y	16.86	3.66	0.11	0.24	9.29	4.58	2.03	Immediate Occupancy
C422 Conf.✓	-X	7.66	3.06	0.05	0.20	8.81	3.83	2.30	Immediate Occupancy
	+X	1.96	2.64	0.01	0.17	8.81	3.30	2.67	Immediate Occupancy
	-Y	0.80	1.64	0.01	0.11	3.55	7.05	0.50	Immediate Occupancy
	+Y	8.49	3.89	0.06	0.26	3.55	8.61	0.41	Immediate Occupancy

FIRM : STA MUH. MUS. LTD. STI.							05-18-2006		PAGE: 22		
PROJECT : guclendirme							(guclendirmel.ST4)				
BEAMS r CAPACITY RATIO											
BEAM	dir	V/ (Ac.fct)	$\rho-\rho' / \rho_{bi}$	$r_i = M_{di} / M_{ri}$	Dmg.	V/ (Ac.fct)	$\rho-\rho' / \rho_{bj}$	$r_j = M_{dj} / M_{rj}$	Dmg.		
BZ01 Conf.✓	-X	0.0510	0.0199	9.73/4.01=2.43	MH	0.0125	-0.0511	4.25/3.31=1.28	MH		
	+X	0.0099	-0.0199	6.7/3.31=2.02	MH	0.0536	0.0511	9.02/5.16=1.75	MH		
BZ02 Conf.✓	-X	0.0508	0.0087	8.39/5.16=1.63	MH	0.0205	0.0225	9.23/4.84=1.91	MH		
	+X	0.0152	-0.0087	5.45/4.84=1.13	MH	0.0455	-0.0225	11.39/4.01=2.84	MH		
BZ04 Conf.✓	-X	0.0764	0.0217	36.42/5.63=6.47	BH	0.0156	-0.0217	26.75/4.88=5.49	BH		
	+X	0.0156	-0.0217	29.6/4.88=6.07	BH	0.0764	0.0217	34.67/5.63=6.16	BH		
BZ05 Conf.✓	-X	0.0930	-0.0173	32.08/5.63=5.7	BH	0.0722	0.0485	28.2/6.27=4.5	BH		
	+X	0.0156	0.0173	26.33/6.27=4.2	BH	0.0052	-0.0485	36.94/4.49=8.23	IH		
BZ06 Conf.✓	-X	0.0695	0.0217	46.14/5.63=8.19	IH	0.0091	-0.0217	39.92/4.84=8.25	IH		
	+X	0.0090	-0.0217	38.8/4.84=8.02	IH	0.0696	0.0217	44.63/5.63=7.92	IH		
BZ07 Conf.✓	-X	0.1254	0.1732	3.26/12.8=0.25	MH	0.1031	-0.3465	0.37/6.52=0.06	MH		
	+X	0.0279	-0.1732	2.74/6.52=0.42	MH	0.0502	0.3465	8.97/18.31=0.49	MH		
BZ07 Conf.✓	-X	0.1596	0.3465	22.11/18.31=1.21	MH	0.1385	-0.3465	26.84/2.94=9.12	IH		
	+X	0.0907	-0.3465	16.74/6.52=2.57	MH	0.1118	0.3465	26.8/8.27=3.24	BH		
BZ08 Conf.✓	-X	0.0436	0.0199	30.18/4.01=7.53	IH	0.0046	-0.0624	22.93/3.28=7.0	IH		
	+X	0.0005	-0.0199	27.01/3.28=8.25	IH	0.0477	0.0624	26.85/5.57=4.82	BH		
BZ09 Conf.✓	-X	0.0472	0.0624	19.63/5.57=3.53	BH	0.0071	-0.0624	12.16/3.28=3.71	BH		
	+X	0.0067	-0.0624	15.39/3.28=4.7	BH	0.0476	0.0624	17.17/5.57=3.08	BH		
BZ10 Conf.✓	-Y	0.0802	0.1732	21.78/9.56=2.28	MH	0.0329	-0.1490	6.1/3.31=1.84	MH		
	+Y	0.0358	0.1732	7.67/3.31=2.31	MH	0.0772	-0.1490	16.85/8.71=1.93	MH		
BZ11 Conf.✓	-Y	0.0545	0.1715	14.92/8.67=1.72	MH	0.0230	-0.0424	11.16/2.45=4.56	BH		
	+Y	0.0064	0.1715	10.85/2.45=4.43	BH	0.0379	-0.0424	13.18/4.01=3.29	BH		
BZ12 Conf.✓	-Y	0.0433	0.0199	15.58/4.01=3.89	BH	0.0023	-0.0624	18.53/3.28=5.66	BH		
	+Y	0.0016	0.0199	13.43/3.28=4.1	BH	0.0471	-0.0624	23.29/5.57=4.18	BH		
BZ13 Conf.✓	-Y	0.0785	0.0217	27.91/5.63=4.95	BH	0.0212	-0.0459	21.32/4.88=4.37	BH		
	+Y	0.0150	0.0217	23.76/4.88=4.87	BH	0.0847	-0.0459	32.68/6.52=5.01	BH		
BZ14 Conf.✓	-Y	0.0729	0.0459	29.66/6.52=4.55	BH	0.0322	0.0225	16.49/4.88=3.38	BH		
	+Y	0.0210	0.0459	24.26/4.88=4.98	BH	0.0617	0.0225	16.59/4.01=4.14	BH		
BZ15 Conf.✓	-Y	0.0577	-0.0225	9.49/4.01=2.37	MH	0.0036	-0.0528	7.28/4.84=1.5	MH		
	+Y	0.0134	-0.0225	8.43/4.84=1.74	MH	0.0674	-0.0528	12.79/6.78=1.89	MH		
BZ16 Conf.✓	-Y	0.1084	0.0069	15.94/6.78=2.35	MH	0.0880	-0.0312	15.94/6.52=2.44	MH		
	+Y	0.0256	0.0069	8.72/6.52=1.34	MH	0.0051	-0.0312	25.58/7.67=3.34	BH		
BZ17 Conf.✓	-Y	0.0706	0.0424	9.87/4.84=2.04	MH	0.0270	-0.0736	8.96/3.28=2.73	MH		
	+Y	0.0257	0.0424	7.15/3.28=2.18	MH	0.0719	-0.0736	19.58/5.98=3.27	BH		
BZ18 Conf.✓	-Y	0.0654	0.0961	34.74/5.98=5.81	BH	0.0276	-0.2824	28.93/2.45=11.82	GB		
	+Y	0.0588	0.0961	31.82/2.45=13.0	GB	0.0966	-0.2824	29.26/12.31=2.38	MH		
BZ21 Conf.✓	-Y	0.0590	-0.0225	25.86/4.01=6.45	BH	0.0222	-0.0217	20.08/4.84=4.15	BH		
	+Y	0.0302	-0.0225	23.75/4.84=4.91	BH	0.0670	-0.0217	22.7/5.63=4.03	BH		
BZ22 Conf.✓	-X	0.0536	0.0511	9.2/5.16=1.79	MH	0.0099	-0.0199	7.26/3.31=2.19	MH		
	+X	0.0125	-0.0511	4.51/3.31=1.36	MH	0.0510	0.0199	10.46/4.01=2.61	MH		
BZ23 Conf.✓	-X	0.0455	-0.0225	11.32/4.01=2.82	MH	0.0152	-0.0087	5.33/4.84=1.1	MH		
	+X	0.0205	0.0225	9.23/4.84=1.91	MH	0.0508	0.0087	8.31/5.16=1.61	MH		
BZ25 Conf.✓	-X	0.0764	0.0217	32.3/5.63=5.73	BH	0.0156	-0.0217	26.76/4.88=5.49	BH		
	+X	0.0156	-0.0217	23.6/4.88=4.84	BH	0.0764	0.0217	31.93/5.63=5.67	BH		
BZ26 Conf.✓	-X	0.0902	-0.0615	36.33/4.01=9.06	IH	0.0566	0.0173	25.1/6.27=4.0	BH		
	+X	0.0105	0.0615	27.76/6.27=4.43	BH	0.0231	-0.0173	31.13/5.63=5.53	BH		
BZ27 Conf.✓	-X	0.0695	0.0217	44.22/5.63=7.85	IH	0.0091	-0.0217	38.28/4.84=7.91	IH		
	+X	0.0090	-0.0217	39.44/4.84=8.15	IH	0.0696	0.0217	45.39/5.63=8.06	IH		
BZ28 Conf.✓	-X	0.1118	0.3465	26.78/8.26=3.24	BH	0.0906	-0.3465	16.72/6.52=2.56	MH		
	+X	0.1385	-0.3465	26.82/2.94=9.11	IH	0.1596	0.3465	22.09/18.31=1.21	MH		
BZ28 Conf.✓	-X	0.1459	0.3465	9.01/18.31=0.49	MH	0.1041	-0.1732	2.56/6.52=0.39	MH		
	+X	0.0127	-0.3465	0.39/6.52=0.06	MH	0.0546	0.1732	3.11/12.8=0.24	MH		
BZ29 Conf.✓	-X	0.0477	0.0624	22.72/5.57=4.08	BH	0.0005	-0.0199	24.99/3.28=7.63	IH		
	+X	0.0046	-0.0624	19.24/3.28=5.87	BH	0.0436	0.0199	28.12/4.01=7.01	IH		

FIRM : STA MUH. MUS. LTD. STI.							05-18-2006		PAGE: 23		
PROJECT : guclendirme							(guclendirme1.ST4)				
BEAM	dir	V/(Ac.fct)	$\rho-\rho'/\rho_{bi}$	$r_i=M_{di}/M_{ri}$	Dmg.	V/(Ac.fct)	$\rho-\rho'/\rho_{bj}$	$r_j=M_{dj}/M_{rj}$	Dmg.		
BZ30 Conf.✓	-X +X	0.0476 0.0071	0.0624 -0.0624	15.54/5.57=2.79 10.6/3.28=3.24	MH BH	0.0067 0.0472	-0.0624 0.0624	11.86/3.28=3.62 16.59/5.57=2.98	BH MH		
BZ31 Conf.✓	-Y +Y	0.0802 0.0358	0.1732 0.1732	22.84/9.56=2.39 9.14/3.31=2.76	MH MH	0.0329 0.0772	-0.1490 -0.1490	6.02/3.31=1.82 16.74/8.71=1.92	MH MH		
BZ32 Conf.✓	-Y +Y	0.0545 0.0064	0.1715 0.1715	13.65/8.67=1.57 9.03/2.45=3.69	MH BH	0.0230 0.0379	-0.0424 -0.0424	10.68/2.45=4.37 12.5/4.01=3.12	BH BH		
BZ33 Conf.✓	-Y +Y	0.0433 0.0016	0.0199 0.0199	15.75/4.01=3.93 13.82/3.28=4.22	BH BH	0.0023 0.0471	-0.0624 -0.0624	18.54/3.28=5.66 23.5/5.57=4.22	BH BH		
BZ34 Conf.✓	-Y +Y	0.0785 0.0150	0.0217 0.0217	28.09/5.63=4.99 23.99/4.88=4.92	BH BH	0.0212 0.0847	-0.0459 -0.0459	21.52/4.88=4.41 32.94/6.52=5.05	BH BH		
BZ35 Conf.✓	-Y +Y	0.0729 0.0210	0.0459 0.0459	28.53/6.52=4.37 22.97/4.88=4.71	BH BH	0.0322 0.0617	0.0225 0.0225	13.88/4.88=2.85 13.31/4.01=3.32	MH BH		
BZ36 Conf.✓	-Y +Y	0.0577 0.0094	-0.0225 -0.0225	7.34/4.01=1.83 5.43/4.84=1.12	MH MH	0.0036 0.0634	-0.0217 -0.0217	6.43/4.84=1.33 11.57/5.63=2.05	MH MH		
BZ37 Conf.✓	-Y +Y	0.1050 0.0255	-0.0243 -0.0243	15.83/5.63=2.81 8.79/6.52=1.35	MH MH	0.0845 0.0051	-0.0312 -0.0312	15.34/6.52=2.35 25.02/7.67=3.26	MH BH		
BZ38 Conf.✓	-Y +Y	0.0706 0.0256	0.0424 0.0424	9.88/4.84=2.04 7.18/3.28=2.19	MH MH	0.0270 0.0720	-0.0736 -0.0736	8.97/3.28=2.74 19.6/5.98=3.28	MH BH		
BZ39 Conf.✓	-Y +Y	0.0653 0.0585	0.0961 0.0961	34.77/5.98=5.82 31.84/2.45=13.01	BH GB	0.0275 0.0964	-0.2824 -0.2824	28.95/2.45=11.82 29.27/12.31=2.38	GB MH		
BZ42 Conf.✓	-X +X	0.0479 0.0032	-0.0650 0.0650	36.63/2.45=14.97 32.92/4.84=6.8	GB IH	0.0032 0.0479	0.0650 -0.0650	32.84/4.84=6.79 36.62/2.45=14.97	IH GB		
BZ43 Conf.✓	-X +X	0.0482 0.0132	-0.0225 0.0225	15.62/4.01=3.9 13.22/4.84=2.73	BH MH	0.0132 0.0482	0.0225 -0.0225	13.19/4.84=2.73 15.66/4.01=3.91	MH BH		
B101 Conf.✓	-X +X	0.0510 0.0099	0.0199 -0.0199	14.47/4.01=3.61 11.35/3.31=3.43	BH BH	0.0125 0.0536	-0.0511 0.0511	7.64/3.31=2.31 12.52/5.16=2.43	MH MH		
B102 Conf.✓	-X +X	0.0527 0.0133	0.0087 -0.0087	11.93/5.16=2.31 9.22/4.84=1.91	MH MH	0.0142 0.0518	0.0225 -0.0225	14.98/4.84=3.1 18.37/4.01=4.58	BH BH		
B104 Conf.✓	-X +X	0.0764 0.0156	0.0217 -0.0217	45.18/5.63=8.02 39.26/4.88=8.05	IH IH	0.0156 0.0764	-0.0217 0.0217	34.62/4.88=7.1 42.31/5.63=7.51	IH IH		
B105 Conf.✓	-X +X	0.0929 0.0172	-0.0173 0.0173	39.1/5.63=6.94 32.39/6.27=5.17	BH BH	0.0721 0.0037	0.0615 -0.0615	36.16/6.27=5.77 44.22/4.01=11.03	BH GB		
B106 Conf.✓	-X +X	0.0696 0.0137	0.0217 -0.0217	54.79/5.63=9.73 47.14/4.84=9.75	IH IH	0.0091 0.0649	0.0225 -0.0225	48.92/4.84=10.11 52.42/4.01=13.08	GB GB		
B107 Conf.✓	-X +X	0.1253 0.0280	0.1732 -0.1732	4.01/12.8=0.31 3.05/6.52=0.47	MH MH	0.1031 0.0503	-0.3465 0.3465	3.71/6.52=0.57 8.75/18.31=0.48	MH MH		
B107 Conf.✓	-X +X	0.1552 0.0782	0.3465 -0.3465	28.47/18.31=1.55 28.85/6.52=4.42	MH BH	0.1341 0.0993	-0.3465 0.3465	27.39/2.3=11.9 36.13/6.47=5.59	GB BH		
B108 Conf.✓	-X +X	0.0436 0.0005	0.0199 -0.0199	33.61/4.01=8.38 30.53/3.28=9.32	IH IH	0.0046 0.0477	-0.0624 0.0624	25.26/3.28=7.71 28.56/5.57=5.13	IH BH		
B109 Conf.✓	-X +X	0.0472 0.0067	0.0624 -0.0624	22.69/5.57=4.07 18.26/3.28=5.57	BH BH	0.0071 0.0476	-0.0624 0.0624	16.24/3.28=4.96 21.38/5.57=3.84	BH BH		
B110 Conf.✓	-Y +Y	0.0790 0.0365	0.1490 0.1490	27.56/8.71=3.16 14.81/3.31=4.47	BH BH	0.0351 0.0776	-0.1490 -0.1490	9.73/3.31=2.94 20.83/8.71=2.39	MH MH		
B111 Conf.✓	-Y +Y	0.0545 0.0064	0.1715 0.1715	17.63/8.67=2.03 12.61/2.45=5.15	MH BH	0.0230 0.0379	-0.0424 -0.0424	13.47/2.45=5.51 14.94/4.01=3.73	BH BH		
B112 Conf.✓	-Y +Y	0.0433 0.0016	0.0199 0.0199	19.38/4.01=4.84 17.58/3.28=5.37	BH BH	0.0023 0.0471	-0.0624 -0.0624	25.6/3.28=7.82 31.56/5.57=5.67	IH BH		
B113 Conf.✓	-Y +Y	0.0819 0.0158	0.0459 0.0459	38.84/6.52=5.96 34.55/4.88=7.09	BH IH	0.0194 0.0855	-0.0459 -0.0459	31.36/4.88=6.43 43.82/6.52=6.72	BH BH		
B114 Conf.✓	-Y +Y	0.0729 0.0210	0.0459 0.0459	36.59/6.52=5.61 31.71/4.88=6.5	BH BH	0.0322 0.0617	0.0225 0.0225	19.82/4.88=4.06 19.55/4.01=4.88	BH BH		
B115 Conf.✓	-Y +Y	0.0577 0.0094	-0.0225 -0.0225	12.05/4.01=3.01 10.21/4.84=2.11	BH MH	0.0036 0.0634	-0.0217 -0.0217	10.52/4.84=2.17 15.21/5.63=2.7	MH MH		
B116 Conf.✓	-Y +Y	0.1097 0.0268	-0.0243 -0.0243	17.59/5.63=3.12 10.61/6.52=1.63	BH MH	0.0893 0.0064	-0.0624 -0.0624	24.69/6.52=3.79 36.5/8.81=4.14	BH BH		

BEAM	dir	V/(Ac.fct)	$\rho-\rho'/\rho_{bi}$	$r_i=M_{di}/M_{ri}$	Dmg.	V/(Ac.fct)	$\rho-\rho'/\rho_{bj}$	$r_j=M_{dj}/M_{rj}$	Dmg.
B421 Conf.✓	-Y +Y	0.0592 0.0244	-0.0225 -0.0225	24.38/4.01=6.08 21.63/4.84=4.47	BH BH	0.0174 0.0662	-0.0217 -0.0217	21.78/4.84=4.5 22.84/5.63=4.06	BH BH
B422 Conf.✓	-X +X	0.0465 0.0164	0.0199 -0.0199	8.93/2.44=3.66 4.62/1.8=2.57	BH MH	0.0170 0.0471	-0.0199 0.0199	7.28/3.31=2.2 9.53/4.01=2.38	MH MH
B423 Conf.✓	-X +X	0.0386 0.0047	0.0424 -0.0424	11.73/3.59=3.27 7.8/2.45=3.19	BH BH	0.0001 0.0339	-0.0424 0.0424	3.08/1.49=2.07 5.99/2.17=2.76	MH MH
B425 Conf.✓	-X +X	0.0733 0.0201	0.0217 -0.0217	23.48/4.2=5.59 15.11/4.2=3.6	BH BH	0.0222 0.0754	-0.0217 0.0217	19.08/4.88=3.91 24.73/5.63=4.39	BH BH
B426 Conf.✓	-X +X	0.0847 0.0253	-0.0615 0.0615	11.54/3.83=3.01 7.88/3.18=2.48	BH MH	0.0500 0.0094	0.0173 -0.0173	7.75/4.67=1.66 14.38/4.85=2.97	MH MH
B427 Conf.✓	-X +X	0.0614 0.0161	0.0199 -0.0199	19.93/4.01=4.97 17.26/3.28=5.27	BH BH	0.0204 0.0657	-0.0624 0.0624	15.39/3.28=4.7 22.85/5.57=4.1	BH BH
B428 Conf.✓	-X +X	0.0488 0.0647	0.3465 -0.3465	11.3/2.41=4.69 6.18/0.86=7.2	BH IH	0.0274 0.0862	-0.3465 0.3465	9.9/3.27=3.03 14.07/9.81=1.43	BH MH
B428 Conf.✓	-X +X	0.1133 0.0016	0.3465 -0.3465	7.47/9.17=0.81 0.18/3.5=0.05	MH MH	0.0715 0.0435	-0.1732 0.1732	1.74/6.52=0.27 2.15/12.8=0.17	MH MH
B429 Conf.✓	-X +X	0.0400 0.0104	0.0624 -0.0624	8.13/2.63=3.09 5.14/1.52=3.38	BH BH	0.0089 0.0385	-0.0199 0.0199	9.1/3.28=2.78 11.62/3.79=3.06	MH BH
B430 Conf.✓	-X +X	0.0364 0.0180	0.0624 -0.0624	10.35/2.43=4.27 4.45/1.43=3.12	BH BH	0.0180 0.0363	-0.0624 0.0624	6.17/1.55=3.99 9.36/2.59=3.62	BH BH
B431 Conf.✓	-Y +Y	0.0753 0.0388	0.0312 0.0312	18.37/7.67=2.4 6.97/6.56=1.06	MH MH	0.0388 0.0753	-0.0624 -0.0624	3.28/2.26=1.45 13.87/4.19=3.31	MH BH
B432 Conf.✓	-Y +Y	0.0314 0.0042	0.1732 0.1732	9.62/3.01=3.19 4.33/1.16=3.73	BH BH	0.0001 0.0274	-0.0424 -0.0424	3.91/1.45=2.71 6.21/2.17=2.86	MH MH
B433 Conf.✓	-Y +Y	0.0390 0.0078	0.0199 0.0199	7.2/2.37=3.04 5.21/1.78=2.93	BH MH	0.0079 0.0390	-0.0199 -0.0199	11.15/3.28=3.4 15.72/4.01=3.92	BH BH
B434 Conf.✓	-Y +Y	0.0718 0.0274	-0.0225 -0.0225	18.05/4.01=4.5 15.78/4.88=3.24	BH BH	0.0383 0.0826	-0.0217 -0.0217	7.66/3.28=2.34 21.77/3.56=6.12	MH BH
B435 Conf.✓	-Y +Y	0.0526 0.0018	0.0217 0.0217	15.2/3.79=4.01 3.59/3.08=1.17	BH MH	0.0090 0.0455	0.0225 0.0225	6.66/2.44=2.73 3.39/2.07=1.64	MH MH
B436 Conf.✓	-Y +Y	0.0406 0.0094	-0.0225 -0.0225	4.02/2.0=2.01 5.82/2.49=2.34	MH MH	0.0141 0.0454	-0.0459 -0.0459	2.08/1.87=1.11 8.79/2.63=3.34	MH BH
B437 Conf.✓	-Y +Y	0.0903 0.0467	0.0624 0.0624	7.05/2.53=2.79 -0.38/1.71=-0.22	MH MH	0.0691 0.0254	-0.0624 -0.0624	10.94/4.23=2.59 19.3/6.52=2.96	MH MH
B439 Conf.✓	-Y +Y	0.0571 0.0230	0.0537 0.0537	16.78/3.85=4.36 15.51/2.45=6.34	BH BH	0.0120 0.0682	-0.1091 -0.1091	46.01/2.45=18.8 48.22/6.45=7.47	GB IH
B442 Conf.✓	-X +X	0.0659 0.0162	-0.0650 0.0650	73.4/2.45=30.0 67.52/4.84=13.96	GB GB	0.0440 0.0058	0.0650 -0.0650	67.53/4.84=13.96 73.38/2.45=29.99	GB GB
B443 Conf.✓	-X +X	0.0630 0.0002	-0.0225 0.0225	14.83/4.01=3.7 10.7/4.33=2.47	BH MH	0.0500 0.0132	0.0225 -0.0225	10.74/4.33=2.48 14.79/4.01=3.69	MH BH

**BUILDING PERFORMANCE**

BEAMS DAMAGE PERCENTAGE

Story NO	(-X)				(X)				(-Y)				(Y)			
	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC
5	3.0	15.0	1.0	1.0	4.0	14.0	1.0	1.0	6.9	10.3	0.0	2.3	4.6	12.6	2.3	0.0
4	2.0	14.0	2.0	2.0	2.0	14.0	2.0	2.0	5.7	10.3	1.1	2.3	4.6	14.9	0.0	0.0
3	3.0	12.0	1.0	4.0	3.0	11.0	3.0	3.0	4.6	11.5	1.1	2.3	5.7	12.6	0.0	1.1
2	2.0	9.0	4.0	5.0	2.0	9.0	4.0	5.0	3.4	10.3	2.3	3.4	2.3	11.5	3.4	2.3
1	6.0	7.0	6.0	1.0	6.0	7.0	6.0	1.0	9.2	10.3	0.0	2.3	4.6	14.9	0.0	2.3
Max.		15.0	6.0	5.0					9.2							

X dir. beams number= 100, Y dir. beams number= 87

**COLUMNS SHEAR PERCENTAGE**

Story NO	(-X)				(X)				(-Y)				(Y)			
	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC
5	94.5	5.5	0.0	0.0	94.4	5.6	0.0	0.0	98.1	1.9	0.0	0.0	98.6	1.4	0.0	0.0
4	96.9	2.5	0.6	0.0	96.7	2.7	0.6	0.0	98.4	1.6	0.0	0.0	98.7	1.3	0.0	0.0
3	96.9	2.5	0.6	0.0	97.0	2.4	0.6	0.0	100.	0.0	0.0	0.0	99.9	0.1	0.0	0.0
2	98.0	1.7	0.3	0.0	97.9	1.8	0.3	0.0	100.	0.0	0.0	0.0	100.	0.0	0.0	0.0
1	99.8	0.2	0.0	0.0	99.8	0.2	0.0	0.0	100.	0.0	0.0	0.0	100.	0.0	0.0	0.0
Max.						5.6	0.6		100.							

**COLUMNS INCLUDE PLASTIC HINGE SHEAR PERCENTAGE**

Story NO	(-X)				(X)				(-Y)				(Y)			
	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC	IO	LS	CP	CC
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	4.4	0.8	0.6	0.0	4.1	0.8	0.6	0.0	2.2	0.0	0.0	0.0	1.5	0.0	0.0	0.0
3	1.6	0.0	0.6	0.0	1.6	0.0	0.6	0.0	1.4	0.0	0.0	0.0	1.3	0.0	0.0	0.0
2	0.5	0.0	0.3	0.0	0.6	0.0	0.3	0.0	0.3	0.0	0.0	0.0	1.0	0.0	0.0	0.0
1	0.4	0.2	0.0	0.0	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.0	0.0
Max.	5.8					1.4	0.6									

Beams Collapse Prevention Damage Ratio=5.0<=20 Collapse Prevention, can need Resistance.  
 Roof Story Vc ratio=0.0<=40  
 Columns include Plastic Hinge Vc ratio=1.4<=30

**REINFORCED PROJECT- EXISTING COLUMN CAPACITY TABLE**

No =  $0,85 \cdot f_{cd} \cdot b \cdot d + f_{yd} \cdot A_s$   
 Nmax =  $0,5 \cdot f_{ck} \cdot A_c$   
 Nd,max = max. design axial load among all load combinations  
 Nd,x/y = axial load for maximum moment (Md,x/y) in x/y dir.  
 Md,x/y = maximum moment in x/y direction  
 Mr,x/y = column capacity moment in x/y dir. (Nd,x/y)  
 Vd,max = max. column shear force among all combinations  
 Vr,max =  $2 \cdot f_{ck}^{1/2} \cdot A_c$   
 Ac = Column section area  
 As,g = Calculated reinf. area  
 As,m = Existing reinf. area  
 rm = Existing reinf. ratio

Existing column min. gross cross section : 0.01  
 Existing column bars corrosion ratio % : 0  
 Exist members checking option : Mr>Md

**ZEMIN. STORY EXIST COLUMN DATA TABLE**

COLUMN NO	SIZE	Ac cm²	EXISTING REINF. end web	Asm cm²	Asg cm²	rm %	No (t)	Nmax (t)	Nd,max (t)	Vd,max (t)
CZ01	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	67.8	4.6
CZ02	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	66.6	2.9
CZ03	60x25	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	48.2	1.1
CZ04	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	6.4	1.3
CZ05	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	5.0	0.5
CZ06	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	89.1	2.5
CZ07	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	89.0	3.5
CZ08	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	6.0	0.9
CZ09	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	73.4	4.1
CZ10	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	100.9	3.9
CZ11	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	43.0	4.1
CZ12	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	80.5	3.0
CZ13	30x70	2100	2x5ø14 + 2x2ø14 (	21.54	21.54	0.010	216.5	126.0	91.7	3.3
CZ14	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	58.2	2.1
CZ15	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	68.2	4.7
CZ16	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	66.2	2.9
CZ17	60x25	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	48.3	1.1
CZ18	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	6.4	1.3
CZ19	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	5.5	0.3
CZ20	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	88.5	3.9
CZ21	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	86.9	3.7
CZ22	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	5.7	0.7
CZ23	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	75.0	4.3
CZ24	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	102.2	4.0
CZ25	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	44.2	4.2
CZ26	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	78.7	3.4

**ZEMIN. STORY X DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd,max/Nmax	+X DIR.					COMMENT	-X DIR.				
		Nd,x (t)	Md,x (tm)	Mr,x (tm)	Md,x/Mr,x	COMMENT		Nd,x (t)	Md,x (tm)	Mr,x (tm)	Md,x/Mr,x	COMMENT
CZ01	0.753	67.8	1.5	6.0	0.254	✓	67.8	1.5	6.0	0.254	✓	
CZ02	0.740	66.1	1.5	6.0	0.248	✓	66.1	1.5	6.0	0.248	✓	
CZ03	0.536	29.0	2.9	13.2	0.220	✓	39.8	2.9	14.2	0.204	✓	
CZ04	0.071	6.4	0.1	3.7	0.039	✓	6.4	0.1	3.7	0.039	✓	
CZ05	0.047	5.0	0.2	11.4	0.015	✓	5.0	0.2	11.4	0.015	✓	
CZ06	0.825	35.9	6.4	16.3	0.392	✓	90.2	6.4	18.0	0.355	✓	
CZ07	0.824	51.7	7.8	17.9	0.440	✓	75.2	7.8	18.5	0.425	✓	
CZ08	0.055	6.0	0.1	5.3	0.027	✓	6.0	0.1	5.3	0.027	✓	
CZ09	0.680	12.2	9.6	12.9	0.743	✓	74.2	9.6	18.5	0.521	✓	
CZ10	0.934	94.5	10.3	17.7	0.583	✓	49.6	10.3	17.7	0.585	✓	
CZ11	0.398	23.8	4.2	6.9	0.604	✓	37.5	4.2	7.7	0.543	✓	
CZ12	0.746	70.3	5.1	8.6	0.590	✓	44.6	5.1	8.1	0.630	✓	
CZ13	0.728	38.7	5.5	8.6	0.638	✓	37.9	5.5	8.5	0.641	✓	
CZ14	0.646	42.2	3.4	5.8	0.589	✓	40.8	3.4	5.7	0.593	✓	
CZ15	0.758	68.2	1.5	6.0	0.256	✓	68.2	1.5	6.0	0.256	✓	
CZ16	0.736	65.9	1.5	6.0	0.247	✓	65.9	1.5	6.0	0.247	✓	
CZ17	0.536	39.8	2.9	14.2	0.207	✓	29.0	2.9	13.2	0.224	✓	
CZ18	0.071	6.4	0.1	3.7	0.039	✓	6.4	0.1	3.7	0.039	✓	
CZ19	0.051	5.5	0.2	11.5	0.016	✓	5.5	0.2	11.5	0.016	✓	
CZ20	0.819	89.6	8.4	18.1	0.466	✓	35.6	8.4	16.3	0.517	✓	
CZ21	0.805	74.1	8.2	18.5	0.442	✓	49.8	8.2	17.7	0.462	✓	
CZ22	0.052	5.7	0.1	5.3	0.026	✓	5.7	0.1	5.3	0.026	✓	
CZ23	0.694	75.8	10.7	18.5	0.579	✓	13.1	10.7	13.1	0.815	✓	
CZ24	0.946	49.7	9.9	17.7	0.561	✓	96.2	9.9	17.6	0.565	✓	
CZ25	0.409	38.0	4.7	7.7	0.608	✓	25.0	4.7	7.0	0.672	✓	
CZ26	0.729	42.7	5.5	8.0	0.691	✓	69.6	5.5	8.6	0.640	✓	

STORY CAPACITY CHECK :  $\frac{112.6}{\sum Nd,max} / \frac{275.4}{\sum Nmax} = 0.409$        $\frac{112.6}{\sum -Md,x} / \frac{275.3}{\sum -Mr,x} = 0.409$   
 $\frac{\sum Nd,max}{\sum Nmax} = 1501.385/2664.0 = 0.564$

**ZEMIN. STORY Y DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd, max/ Nmax	+Y DIR.					COMMENT	-Y DIR.				
		Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y			Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y	
CZ01	0.753	37.2	6.9	14.0	0.489	✓	59.5	6.9	15.0	0.457	✓	
CZ02	0.740	27.0	4.2	12.9	0.322	✓	67.4	4.2	14.9	0.280	✓	
CZ03	0.536	48.2	1.1	5.9	0.195	✓	48.2	1.1	5.9	0.195	✓	
CZ04	0.071	6.4	0.5	9.9	0.055	✓	6.4	0.5	9.9	0.055	✓	
CZ05	0.047	5.0	0.2	5.2	0.031	✓	5.0	0.2	5.2	0.031	✓	
CZ06	0.825	35.9	3.9	7.6	0.506	✓	90.2	3.9	8.4	0.461	✓	
CZ07	0.824	89.0	2.1	8.4	0.253	✓	89.0	2.1	8.4	0.253	✓	
CZ08	0.055	6.0	0.6	11.6	0.055	✓	6.0	0.6	11.6	0.055	✓	
CZ09	0.680	12.2	3.3	6.0	0.559	✓	74.2	3.3	8.6	0.386	✓	
CZ10	0.934	100.9	2.4	7.8	0.310	✓	100.9	2.4	7.8	0.310	✓	
CZ11	0.398	23.8	9.4	14.9	0.633	✓	37.5	9.4	16.5	0.570	✓	
CZ12	0.746	70.3	5.6	18.5	0.304	✓	44.6	5.6	17.2	0.326	✓	
CZ13	0.728	92.2	4.3	25.8	0.166	✓	-15.7	4.3	9.3	0.458	✓	
CZ14	0.646	77.1	2.4	14.5	0.164	✓	6.0	2.4	9.8	0.242	✓	
CZ15	0.758	60.5	9.0	15.0	0.597	✓	36.9	9.0	14.0	0.641	✓	
CZ16	0.736	67.0	5.1	14.9	0.341	✓	27.0	5.1	12.9	0.392	✓	
CZ17	0.536	48.3	1.1	5.9	0.193	✓	48.3	1.1	5.9	0.193	✓	
CZ18	0.071	6.4	0.5	9.9	0.054	✓	6.4	0.5	9.9	0.054	✓	
CZ19	0.051	5.5	0.2	5.2	0.034	✓	5.5	0.2	5.2	0.034	✓	
CZ20	0.819	59.9	2.9	8.5	0.341	✓	35.6	2.8	7.6	0.364	✓	
CZ21	0.805	86.9	2.1	8.5	0.246	✓	86.9	2.1	8.5	0.246	✓	
CZ22	0.052	5.7	0.6	11.6	0.050	✓	5.7	0.6	11.6	0.050	✓	
CZ23	0.694	75.8	3.4	8.6	0.398	✓	13.1	3.4	6.0	0.569	✓	
CZ24	0.946	102.2	2.5	7.7	0.317	✓	102.2	2.5	7.7	0.317	✓	
CZ25	0.409	38.0	9.0	16.6	0.543	✓	-25.0	9.0	15.0	0.599	✓	
CZ26	0.729	42.7	4.4	17.0	0.258	✓	37.2	4.6	16.5	0.278	✓	

STORY CAPACITY CHECK : 87.6 292.5 87.7 269.5  
 $\sum Md, y / \sum Mr, y = 0.300$   $\sum -Md, y / \sum -Mr, y = 0.325$   
 $\sum Nd, max / \sum Nmax = 1501.385 / 2664.0 = 0.564$

**1. NORMAL. STORY EXIST COLUMN DATA TABLE**

COLUMN NO	SIZE	Ac cm <sup>2</sup>	EXISTING REINF. end web	Asm cm <sup>2</sup>	Asg cm <sup>2</sup>	rm %	No (t)	Nmax (t)	Nd, max (t)	Vd, max (t)
C101	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	54.5	4.3
C102	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	53.0	5.1
C103	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	37.6	4.3
C104	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	3.2	1.2
C105	50x30	1500	2x4ø14 + 2x1ø14 (	15.39	15.39	0.010	154.6	90.0	2.6	0.9
C106	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	71.2	7.3
C107	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	71.0	10.2
C108	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	3.0	1.3
C109	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	58.0	8.7
C110	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	81.4	8.2
C111	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	34.7	5.4
C112	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	21.54	0.010	185.6	108.0	65.0	6.3
C113	30x70	2100	2x5ø14 + 2x2ø14 (	21.54	36.17	0.010	216.5	126.0	89.6	7.7
C114	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	62.3	3.7
C115	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	54.9	5.7
C116	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	52.7	5.1
C117	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	37.6	4.3
C118	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	3.2	1.1
C119	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	3.1	1.3
C120	50x30	1500	2x4ø14 + 2x1ø14 (	15.39	15.39	0.010	154.6	90.0	71.2	5.4
C121	60x25	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	68.2	9.1
C122	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	15.39	0.010	154.6	90.0	2.7	1.2
C123	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	59.7	7.7
C124	60x30	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	83.0	7.9
C125	30x60	1800	2x4ø14 + 2x2ø14 (	18.46	18.46	0.010	185.6	108.0	35.8	5.3
C126	25x60	1500	2x3ø14 + 2x2ø14 (	15.39	18.46	0.010	154.6	90.0	63.1	5.9

**1. NORMAL. STORY X DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd, max/ Nmax	+X DIR.					COMMENT	-X DIR.				
		Nd, x (t)	Md, x (tm)	Mr, x (tm)	Md, x/ Mr, x			Nd, x (t)	Md, x (tm)	Mr, x (tm)	Md, x/ Mr, x	
C101	0.726	30.4	1.4	4.8	0.284	✓	46.6	1.4	5.0	0.269	✓	
C102	0.588	22.7	3.9	5.0	0.789	✓	52.0	3.9	5.9	0.660	✓	
C103	0.501	22.0	6.8	10.5	0.642	✓	30.9	6.8	11.2	0.605	✓	

**2. NORMAL. STORY Y DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd, max/ Nmax	+Y DIR.					COMMENT	-Y DIR.					
		Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y			Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y		
C213	0.394	62.8	5.3	15.0	0.353	✓	-13.1	5.3	5.1	1.029	Mr	×	
C214	0.611	45.8	4.8	11.7	0.412	✓	4.3	4.8	7.8	0.618		✓	
C215	0.547	35.6	6.0	11.4	0.528	✓	22.0	6.0	10.5	0.571		✓	
C216	0.525	38.6	4.5	11.5	0.393	✓	16.5	4.5	9.9	0.459		✓	
C217	0.381	28.6	0.6	4.7	0.137	✓	28.6	0.6	4.7	0.137		✓	
C218	0.632	12.4	6.2	9.3	0.675	✓	21.1	6.2	10.4	0.599		✓	
C219	0.344	10.9	3.1	3.9	0.795	✓	25.2	3.1	4.6	0.681		✓	
C220	0.597	36.7	6.7	6.5	1.029	Mr	×	38.6	6.7	6.6	1.017	Mr	×
C221	0.662	34.4	2.9	4.9	0.594	✓	35.2	2.9	4.9	0.592		✓	
C222	0.434	-3.1	2.6	6.3	0.414	✓	48.6	2.6	11.8	0.222		✓	
C223	0.464	24.8	4.5	5.1	0.878	✓	28.7	4.5	5.3	0.841		✓	
C224	0.701	47.8	4.1	6.9	0.588	✓	40.5	4.1	6.7	0.606		✓	
C225	0.248	24.5	5.9	14.9	0.394	✓	13.0	5.9	13.1	0.449		✓	
C226	0.627	43.5	5.5	11.6	0.473	✓	22.3	5.5	10.6	0.521		✓	

STORY CAPACITY CHECK : 108.8 209.8 109.1 205.9  
 $\sum Md, y / \sum Mr, y = 0.518$   $\sum -Md, y / \sum -Mr, y = 0.530$   
 $\sum Nd, max / \sum Nmax = 1083.38 / 2043.0 = 0.530$

**3. NORMAL. STORY EXIST COLUMN DATA TABLE**

COLUMN NO	SIZE	Ac cm <sup>2</sup>	EXISTING REINF. end web	Asm cm <sup>2</sup>	Asg cm <sup>2</sup>	rm %	No (t)	Nmax (t)	Nd, max (t)	Vd, max (t)
C301	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	27.5	3.7
C302	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	26.1	3.0
C303	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	19.1	3.6
C304	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	14.9	5.1
C305	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	13.6	2.9
C306	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	35.4	4.1
C307	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	33.6	5.3
C308	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	14.6	2.8
C309	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	25.7	5.1
C310	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	41.0	4.3
C311	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	17.2	3.0
C312	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	32.0	3.9
C313	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	24.62	0.012	134.2	75.0	20.6	3.9
C314	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	29.7	3.3
C315	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	27.4	4.0
C316	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	26.1	3.0
C317	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	19.1	3.5
C318	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	13.7	5.0
C319	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	13.9	2.9
C320	50x30	1500	2x4ø14 + 2x1ø14 (	15.39	15.39	0.010	154.6	90.0	36.0	4.3
C321	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	32.2	5.3
C322	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	14.6	2.8
C323	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	25.6	4.7
C324	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	41.8	4.2
C325	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	17.3	2.6
C326	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	31.5	3.8

**3. NORMAL. STORY X DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd, max/ Nmax	+X DIR.					COMMENT	-X DIR.					
		Nd, x (t)	Md, x (tm)	Mr, x (tm)	Md, x/ Mr, x			Nd, x (t)	Md, x (tm)	Mr, x (tm)	Md, x/ Mr, x		
C301	0.366	15.8	1.3	4.2	0.312	✓	22.8	1.3	4.5	0.291		✓	
C302	0.348	12.0	3.5	4.0	0.884	✓	24.6	3.5	4.5	0.776		✓	
C303	0.254	11.0	5.3	9.0	0.590	✓	15.6	5.3	9.7	0.547		✓	
C304	0.199	4.5	0.3	3.4	0.100	✓	14.9	0.3	4.1	0.083		✓	
C305	0.182	8.4	1.9	8.6	0.224	✓	10.6	1.9	9.0	0.214		✓	
C306	0.472	16.5	4.3	9.9	0.433	✓	33.1	4.3	11.3	0.378		✓	
C307	0.448	17.7	8.1	10.0	0.809	✓	29.4	8.1	11.1	0.730		✓	
C308	0.195	13.3	4.2	4.1	1.032	Mr	×	6.3	4.2	3.6	1.168	Mr	×
C309	0.343	9.1	4.2	8.7	0.486	✓	25.7	4.2	10.9	0.388		✓	
C310	0.547	34.4	6.5	11.3	0.574	✓	23.0	6.5	10.7	0.611		✓	
C311	0.229	9.6	2.7	3.8	0.701	✓	14.4	2.7	4.1	0.655		✓	
C312	0.427	25.5	5.0	4.6	1.090	Mr	×	19.3	5.0	4.3	1.153	Mr	×
C313	0.274	14.5	5.9	4.1	1.437	Mr	×	14.3	5.9	4.1	1.441	Mr	×
C314	0.396	16.9	5.0	4.2	1.195	Mr	×	16.9	5.0	4.2	1.194	Mr	×
C315	0.365	22.8	2.7	4.5	0.610	✓	15.6	2.7	4.2	0.655		✓	



**4. NORMAL. STORY EXIST COLUMN DATA TABLE**

COLUMN NO	SIZE	Ac cm <sup>2</sup>	EXISTING REINF. end web	Asm cm <sup>2</sup>	Asg cm <sup>2</sup>	rm %	No (t)	Nmax (t)	Nd,max (t)	Vd,max (t)
C422	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	6.0	2.7
C423	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	12.2	5.3
C424	50x25	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	21.6	3.9
C425	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	15.39	0.012	134.2	75.0	8.4	3.5
C426	25x50	1250	2x4ø14 + 2x1ø14 (	15.39	18.46	0.012	134.2	75.0	15.6	4.6

**4. NORMAL. STORY X DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd,max/Nmax	+X DIR.					COMMENT	-X DIR.					COMMENT
		Nd,x (t)	Md,x (tm)	Mr,x (tm)	Md,x/Mr,x	Nd,x (t)		Md,x (tm)	Mr,x (tm)	Md,x/Mr,x			
C401	0.180	8.2	1.5	3.7	0.399	✓	10.8	1.5	3.9	0.380	✓		
C402	0.176	6.7	3.9	3.6	1.072	Mr ✗	11.8	3.9	4.0	0.975	✓		
C403	0.125	5.6	6.5	8.1	0.805	✓	7.6	6.5	8.4	0.770	✓		
C404	0.097	7.3	0.2	3.7	0.045	✓	2.8	0.2	3.3	0.050	✓		
C405	0.128	-0.8	1.0	6.7	0.148	✓	9.6	1.0	8.8	0.114	✓		
C406	0.240	9.5	4.4	8.8	0.503	✓	15.7	4.4	9.7	0.453	✓		
C407	0.224	8.9	8.6	8.7	0.991	✓	14.7	8.6	9.6	0.896	✓		
C408	0.084	6.3	4.2	3.6	1.173	Mr ✗	2.0	4.2	3.2	1.302	Mr ✗		
C409	0.161	12.1	4.5	9.2	0.490	✓	12.1	4.5	9.2	0.490	✓		
C410	0.284	16.9	6.6	9.9	0.670	✓	12.9	6.6	9.3	0.711	✓		
C411	0.111	5.0	1.9	3.5	0.548	✓	6.7	1.9	3.6	0.527	✓		
C412	0.212	12.2	4.2	4.0	1.042	Mr ✗	10.0	4.2	3.9	1.078	Mr ✗		
C413	0.111	5.9	5.1	3.6	1.438	Mr ✗	5.8	5.1	3.5	1.442	Mr ✗		
C414	0.179	8.5	4.4	3.8	1.171	Mr ✗	8.5	4.4	3.8	1.170	Mr ✗		
C415	0.180	10.7	3.4	3.9	0.865	✓	8.2	3.4	3.7	0.907	✓		
C416	0.175	11.7	2.3	4.0	0.590	✓	6.7	2.3	3.6	0.649	✓		
C417	0.125	7.6	6.7	8.4	0.793	✓	5.6	6.7	8.1	0.830	✓		
C418	0.096	7.2	0.2	3.7	0.044	✓	7.2	0.2	3.7	0.044	✓		
C419	0.128	9.6	1.0	8.8	0.112	✓	-0.7	1.0	6.8	0.146	✓		
C420	0.204	16.1	8.3	10.0	0.833	✓	9.6	8.3	8.9	0.938	✓		
C421	0.216	14.0	8.1	9.5	0.853	✓	8.7	8.1	8.6	0.939	✓		
C422	0.080	4.8	2.8	3.5	0.819	✓	3.7	2.8	3.4	0.841	✓		
C423	0.163	11.3	8.9	9.1	0.978	✓	5.8	8.9	8.1	1.095	Mr ✗		
C424	0.288	13.1	5.4	9.4	0.581	✓	17.2	5.4	10.0	0.547	✓		
C425	0.112	6.7	4.2	3.6	1.157	Mr ✗	5.0	4.2	3.5	1.202	Mr ✗		
C426	0.208	9.9	4.5	3.9	1.171	Mr ✗	11.9	4.5	4.0	1.134	Mr ✗		

STORY CAPACITY CHECK : 112.8 158.4 112.8 156.5  
 $\sum +Md,x / \sum +Mr,x = 0.712$   $\sum -Md,x / \sum -Mr,x = 0.721$   
 $\sum Nd,max / \sum Nmax = 324.737 / 1965.0 = 0.165$

**4. NORMAL. STORY Y DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd,max/Nmax	+Y DIR.					COMMENT	-Y DIR.					COMMENT
		Nd,y (t)	Md,y (tm)	Mr,y (tm)	Md,y/Mr,y	Nd,y (t)		Md,y (tm)	Mr,y (tm)	Md,y/Mr,y			
C401	0.180	13.5	7.5	9.4	0.794	✓	13.5	7.5	9.4	0.794	✓		
C402	0.176	7.6	4.5	8.4	0.534	✓	10.9	4.5	9.0	0.500	✓		
C403	0.125	6.1	0.2	3.6	0.066	✓	7.1	0.2	3.6	0.064	✓		
C404	0.097	4.2	8.0	7.8	1.027	Mr ✗	5.9	8.0	8.1	0.986	✓		
C405	0.128	2.9	4.5	3.3	1.365	Mr ✗	5.9	4.5	3.5	1.272	Mr ✗		
C406	0.240	13.0	5.2	4.0	1.288	Mr ✗	12.2	5.2	4.0	1.300	Mr ✗		
C407	0.224	8.8	2.5	3.8	0.662	✓	14.8	2.5	4.1	0.606	✓		
C408	0.084	3.7	1.2	7.7	0.153	✓	3.6	1.2	7.7	0.150	✓		
C409	0.161	7.7	3.6	3.7	0.968	✓	9.2	3.6	3.8	0.937	✓		
C410	0.284	16.0	2.5	4.2	0.591	✓	13.8	2.5	4.1	0.605	✓		
C411	0.111	7.1	6.1	8.3	0.726	✓	4.6	6.1	7.9	0.770	✓		
C412	0.212	13.8	8.2	9.5	0.861	✓	8.4	8.2	8.6	0.951	✓		
C413	0.111	17.1	5.2	9.9	0.524	✓	-5.3	5.2	5.8	0.896	✓		
C414	0.179	13.4	6.4	9.4	0.678	✓	3.6	6.4	7.7	0.832	✓		
C415	0.180	10.9	7.1	9.0	0.792	✓	8.0	7.1	8.5	0.840	✓		
C416	0.175	7.6	4.3	8.4	0.515	✓	6.6	4.6	8.3	0.552	✓		
C417	0.125	6.1	0.2	3.6	0.065	✓	7.1	0.2	3.6	0.063	✓		
C418	0.096	4.2	7.7	7.8	0.993	✓	5.9	7.7	8.1	0.953	✓		
C419	0.128	3.0	4.4	3.3	1.343	Mr ✗	5.9	4.4	3.6	1.253	Mr ✗		
C420	0.204	13.1	7.3	5.2	1.404	Mr ✗	12.6	7.3	5.2	1.416	Mr ✗		
C421	0.216	10.6	1.9	3.9	0.497	✓	12.1	1.9	4.0	0.486	✓		
C422	0.080	3.8	1.2	7.7	0.151	✓	4.7	1.2	7.9	0.147	✓		
C423	0.163	8.1	3.5	3.7	0.950	✓	9.0	3.5	3.8	0.931	✓		
C424	0.288	16.3	2.4	4.2	0.566	✓	14.0	2.4	4.1	0.581	✓		

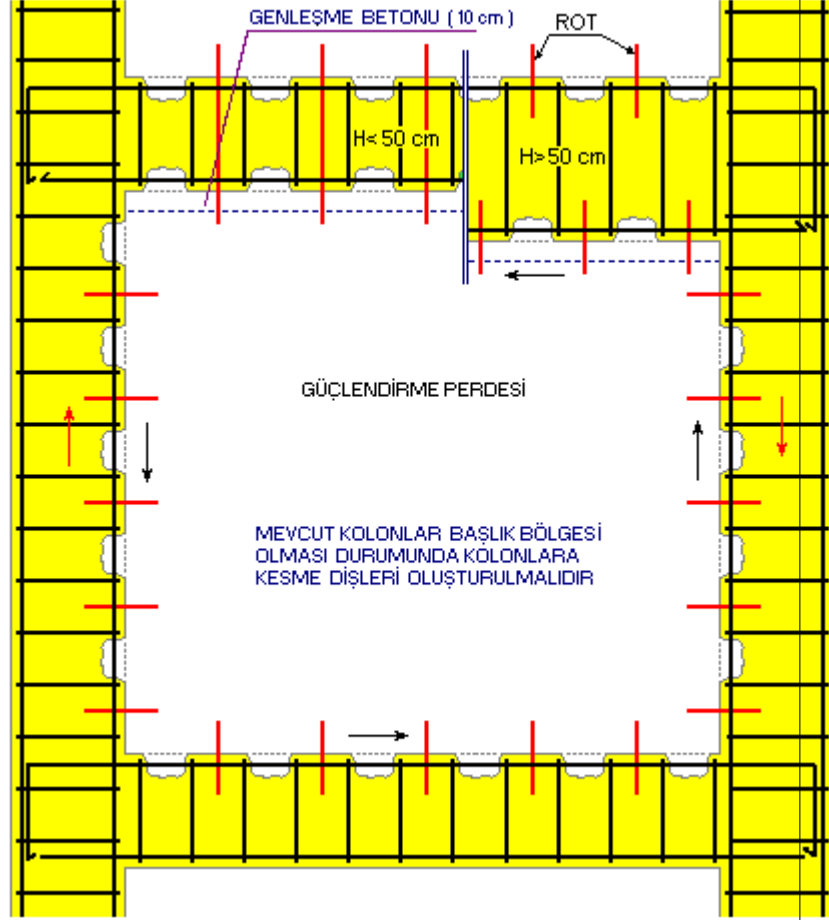
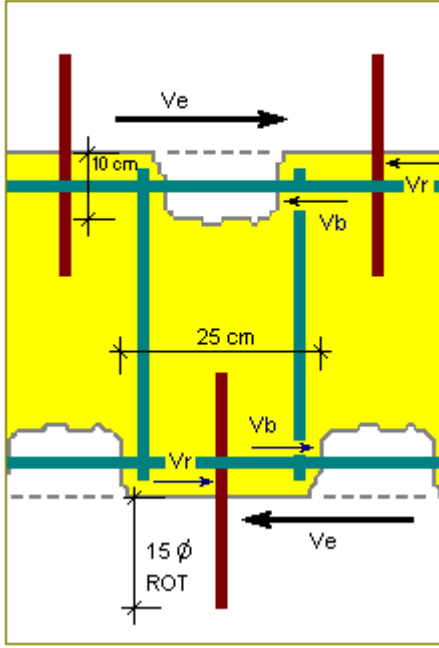
**4. NORMAL. STORY Y DIR. EXISTING COLUMN CAPACITY SCHUDULE**

COLUMN NO	Nd, max/ Nmax	+Y DIR.					-Y DIR.				
		Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y	COMMENT	Nd, y (t)	Md, y (tm)	Mr, y (tm)	Md, y/ Mr, y	COMMENT
C425	0.112	7.1	5.9	8.4	0.712	✓	4.6	5.9	7.9	0.755	✓
C426	0.208	13.5	7.8	9.4	0.831	✓	8.3	7.8	8.6	0.915	✓

STORY CAPACITY CHECK :

	119.5	167.7	119.6	160.8
	$\sum +Md, y / \sum +Mr, y =$	0.712	$\sum -Md, y / \sum -Mr, y =$	0.744
	$\sum Nd, max / \sum Nmax =$	324.737 / 1965.0 =		0.165

## ROT ve KESME dişlerinin hesabı



SHEAR CHECK FOR RETROFITTED SHEARWALL  
C12

$f_{cd} = 96.$   $f_{ctd} = 9.69$  (kg/cm<sup>2</sup>)  
 $f_{yd} = 4000.$  (kg/cm<sup>2</sup>)

Rod shear force capacity :  
 $V_r = 1.49$  (t)  $\phi 20$   $l = 597$  mm

## PZ03 SHEAR CHECK IN PANEL RETROFITTING

shear force capacity for single rib:

$V_{c1} = 96. \times 20. \times 5 = 9.6$  (t)  $V_{c2} = 0.65 \times 9.69 \times 20. \times 25 = 3.15$  (t) >>  $V_b = 3.15$  (t)

shear check for column conn. :  $V_{py} = 18.74$  (t)

shear force capacity of edge column :  $V_k = 0.65 \times 9.69 \times 1500. = 9.45$  (t)

Column reinf. =  $1\phi 14$   $A_s = 1.54$  cm<sup>2</sup>

$V = 5 \times 3.15$  (rib) +  $5 \times 1.49$  (rod) +  $6.16$  (reinf.) =  $29.37 > 18.74$  (t)

shear check for beam connection:  $V_{px} = 94.9$  (t)

Friction force =  $1.4 \times (N_g - N_e) = 30.8$  (t)

$V = 4 \times 3.15$  (rib) +  $29 \times 1.49$  (rod) +  $9.45$  (colum) +  $30.8$  (friction) =  $96.13 > 94.9$  (t)

## PZ24 SHEAR CHECK IN PANEL RETROFITTING

shear force capacity for single rib:

$V_{c1} = 96. \times 20. \times 5 = 9.6$  (t)  $V_{c2} = 0.65 \times 9.69 \times 20. \times 25 = 3.15$  (t) >>  $V_b = 3.15$  (t)

shear check for column conn. :  $V_{py} = 18.77$  (t)

shear force capacity of edge column :  $V_k = 0.65 \times 9.69 \times 1500. = 9.45$  (t)

Column reinf. =  $1\phi 14$   $A_s = 1.54$  cm<sup>2</sup>

$V = 5 \times 3.15$  (rib) +  $5 \times 1.49$  (rod) +  $6.16$  (reinf.) =  $29.37 > 18.77$  (t)

shear check for beam connection:  $V_{px} = 95.35$  (t)

Friction force =  $1.4 \times (N_g - N_e) = 29.82$  (t)

$V = 4 \times 3.15$  (rib) +  $30 \times 1.49$  (rod) +  $9.45$  (colum) +  $29.82$  (friction) =  $96.64 > 95.35$  (t)

## P103 SHEAR CHECK IN PANEL RETROFITTING

shear force capacity for single rib:

$V_{c1} = 96. \times 20. \times 5 = 9.6$  (t)  $V_{c2} = 0.65 \times 9.69 \times 20. \times 25 = 3.15$  (t) >>  $V_b = 3.15$  (t)

shear check for column conn. :  $V_{py} = 112.43$  (t)

shear force capacity of edge column :  $V_k = 0.65 \times 9.69 \times 1500. = 9.45$  (t)

Column reinf. =  $1\phi 14$   $A_s = 1.54$  cm<sup>2</sup>

$V = 5 \times 3.15$  (rib) +  $61 \times 1.49$  (rod) +  $6.16$  (reinf.) =  $112.95 > 112.43$  (t)

shear check for beam connection:  $V_{px} = 41.93$  (t)

Friction force =  $1.4 \times (N_g - N_e) = -2.15$  (t)

$V = 4 \times 3.15$  (rib) +  $15 \times 1.49$  (rod) +  $9.45$  (colum) +  $-2.15$  (friction) =  $42.29 > 41.93$  (t)

**P124 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=111.55 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1500.=9.45$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $61x1.49$  (rod)+6.16 (reinf.) =112.95>111.55 (t)  
**shear check for beam connection: Vpx=40.2 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = -1.93$  (t)  
 $V=4x3.15$  (rib)+ $14x1.49$  (rod)+9.45 (column) + $-1.93$  (friction) =41.02>40.2 (t)

**P203 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=37.21 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $11x1.49$  (rod)+6.16 (reinf.) =38.33>37.21 (t)  
**shear check for beam connection: Vpx=68.51 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 42.16$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +42.16 (friction) =68.6>68.51 (t)

**P224 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=37.66 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $11x1.49$  (rod)+6.16 (reinf.) =38.33>37.66 (t)  
**shear check for beam connection: Vpx=67.1 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 43.14$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +43.14 (friction) =69.59>67.1 (t)

**P303 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=22.48 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $5x1.49$  (rod)+6.16 (reinf.) =29.37>22.48 (t)  
**shear check for beam connection: Vpx=45.81 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 31.38$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +31.38 (friction) =57.83>45.81 (t)

**P324 SHEAR CHECK IN PANEL REFROFITTING**

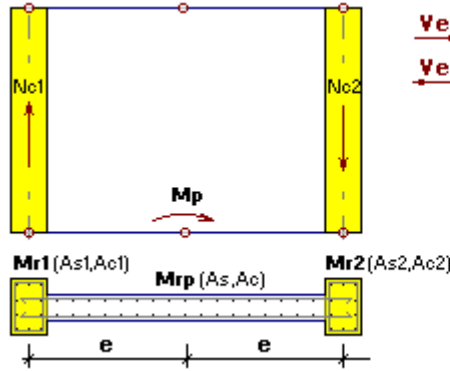
shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=22.53 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $5x1.49$  (rod)+6.16 (reinf.) =29.37>22.53 (t)  
**shear check for beam connection: Vpx=46. (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 31.87$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +31.87 (friction) =58.32>46. (t)

**P403 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=11.2 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $5x1.49$  (rod)+6.16 (reinf.) =29.37>11.2 (t)  
**shear check for beam connection: Vpx=15.33 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 16.33$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +16.33 (friction) =42.77>15.33 (t)

**P424 SHEAR CHECK IN PANEL REFROFITTING**

shear force capacity for single rib:  
 $Vc1=96.x20.x5=9.6$  (t)      $Vc2=0.65x9.69x20.x25=3.15$  (t)     >>  $Vb=3.15$  (t)  
**shear check for column conn. : Vpy=11.18 (t)**  
 shear force capacity of edge column :  $Vk=0.65 \times 9.69 \times 1250.=7.88$  (t)  
 Column reinf. = $\phi 14$  As=1.54 cm<sup>2</sup>  
 $V=5x3.15$  (rib)+ $5x1.49$  (rod)+6.16 (reinf.) =29.37>11.18 (t)  
**shear check for beam connection: Vpx=15.38 (t)**  
 Friction force =  $1.4 \times (Ng - Ne) = 16.51$  (t)  
 $V=4x3.15$  (rib)+ $4x1.49$  (rod)+7.88 (column) +16.51 (friction) =42.96>15.38 (t)



$\vec{v}e$   $M_{r1} = A_{s1} f_{yd} e$ ,  $M_{r2} = 0.85 A_{c2} f_{cd} + A_{s2} f_{yd} e$

$\overleftarrow{v}e$   $M_{r1} = 0.85 A_{c1} f_{cd} + A_{s1} f_{yd} e$ ,  $M_{r2} = A_{s2} f_{yd} e$

$M_d = (M_{c1} + N_{c1} \times e) + (M_{c2} + N_{c2} \times e) + M_p$

$M_r = M_{rp} + M_{r1} + M_{r2} > M_d$

$g_{sh} = \frac{2 \cdot A_{sWS}}{A_{ch}} \frac{L_w}{s}$   $V_r = 0.22 A_{ch} f_{cd} > V_d$

$V_r = 0.65 f_{ctd} A_c + g_{sh} A_{ch} f_{yd} > V_d$

**PANEL MOMENT and SHEAR CAPACITY CHECK (tm)**

Panel	Com.	Mp	Mc1	Mc2	Mrp	Mr1	Mr2	ΣMd	ΣMr	Vd	Vr	✓, ✗
PZ03	10	-325.17	-322.31	0.00	155.63	1016.95	56.96	647.48	1229.55	95.00	154.87	✓
PZ19	12	536.35	207.06	113.76	397.24	377.67	382.57	857.16	1157.48	138.66	146.60	✓
PZ24	10	325.22	319.85	0.00	156.57	870.81	200.64	645.07	1228.02	95.40	154.87	✓
PZ40	11	538.15	206.22	113.43	397.42	377.67	382.57	857.80	1157.66	139.88	146.60	✓
P103	10	-117.22	-348.11	0.00	102.11	1127.89	47.47	465.32	1277.47	44.31	125.43	✓
P119	12	136.29	224.84	201.15	233.47	468.08	405.61	562.28	1107.16	57.45	146.60	✓
P124	10	113.81	341.69	0.00	86.74	962.70	200.64	455.50	1250.08	41.96	122.60	✓
P140	11	146.32	223.05	199.96	233.38	454.22	405.61	569.33	1093.21	59.29	146.60	✓
P203	10	163.04	40.26	26.05	135.97	43.44	197.66	229.34	377.07	71.38	96.87	✓
P219	12	-217.41	-56.00	-53.30	324.91	285.25	93.28	326.71	703.44	93.17	148.58	✓
P224	10	-159.14	-27.03	-41.32	136.58	197.66	43.44	227.49	377.69	70.38	96.87	✓
P240	11	-210.60	-54.91	-52.37	324.91	285.25	93.28	317.88	703.44	90.42	148.58	✓
P303	10	73.03	7.03	-1.62	127.13	43.44	197.66	78.43	368.24	48.22	96.87	✓
P319	11	-97.91	-11.61	-12.90	306.90	285.25	93.28	122.42	685.43	63.57	148.58	✓
P324	10	-72.89	1.41	-7.18	127.41	197.66	43.44	78.65	368.52	48.54	96.87	✓
P340	12	-97.96	-11.47	-12.77	306.96	285.25	93.28	122.21	685.49	62.98	148.58	✓
P403	10	48.31	-3.01	-7.68	114.57	43.44	197.66	37.62	355.67	18.39	96.87	✓
P419	11	-54.34	-0.98	-0.50	274.58	285.25	93.28	55.82	653.12	26.30	148.58	✓
P424	10	-48.64	7.64	2.99	114.73	197.66	43.44	38.01	355.84	18.74	96.87	✓
P440	12	-54.21	-0.93	-0.44	274.61	285.25	93.28	55.59	653.15	26.50	148.58	✓